

NASA Contractor Report 191549, Volume 2

1N-04
198142
P. 51

PARALLEL RUNWAY REQUIREMENT ANALYSIS STUDY

Volume 2 - Simulation Manual

Y.S. Ebrahimi and K.S. Chun

BOEING COMMERCIAL AIRPLANE GROUP
Seattle, Washington

Contract NAS1-18027
December 1993



National Aeronautics and
Space Administration

Langley Research Center
Hampton, Virginia 23681-0001

N94-22278

Unclass

G3/04 0198142

(NASA-CR-191549-Vol-2) PARALLEL
RUNWAY REQUIREMENT ANALYSIS STUDY-
VOLUME 2: SIMULATION MANUAL Final
Report (Boeing Commercial Airplane
Co.) 51 p

NASA Contractor Report 191549, Volume 2

PARALLEL RUNWAY REQUIREMENT ANALYSIS STUDY

Volume 2 - Simulation Manual

Y.S. Ebrahimi and K.S. Chun

**BOEING COMMERCIAL AIRPLANE GROUP
Seattle, Washington**

**Contract NAS1-18027
December 1993**



National Aeronautics and
Space Administration

Langley Research Center
Hampton, Virginia 23681-0001

CONTENTS

	Page
1.0 SUMMARY	1
2.0 INTRODUCTION	2
2.1 Background	2
2.2 Precision Runway Monitor System	4
2.3 PLAND_BLUNDER Simulation Program	6
2.3.1 Assumptions and Limitations	6
2.3.2 Input(s) Parameters of Simulation	7
2.3.3 Output of Simulation	7
3.0 SYMBOLS AND ABBREVIATIONS	8
4.0 RUNNING THE PROGRAM	9
4.1 Software Installation and Information to Build PLB Simulation	9
4.2 Input File	9
4.2.1 Overview of Commands for the PLB Simulation	9
4.2.1.1 Definition of Commands and Parameters	11
4.2.2 Description of Profiles	11
4.2.3 Interpretation of Input File	12
4.2.3.1 Aircraft Types and Fleetmix	13
4.2.3.2 Runway Geometry	14
4.2.3.3 Define Alarm Criteria	14
4.2.3.4 Response Delay Times	15
4.2.3.5 Blunder and Escape Profiles For Aircraft	16
4.2.3.6 Range of X-offset Geometries and Number of Runs	17
4.3 Running PLB Simulation	18
4.4 PLB Simulation Outputs	18
4.4.1 run_rec.track Output File	18
4.4.2 AC_1.track Output File	20
4.4.3 AC_2.track Output File	21
4.4.4 RUN.track Output File	21
4.5 Analysis of Data Output	22
4.5.1 Statistical Analysis of Output Data	22
APPENDIX A - REFERENCE MANUAL	27
APPENDIX B - OUTPUT FILES	34
BIBLIOGRAPHY	46

PRECEDING PAGE BLANK NOT FILMED

LIST OF FIGURES

	Page
1. Parallel Runway Approach Zones	3
2. Normal Operating Zone Shrinks as Runway Separation is Reduced	5
3. Blunder-Model Event Sequence	5
4. PBL Flow Diagram	23
5. Plot of stats.stat	26

LIST OF TABLES

	Page
1. Sample PLAND_EXEC.DAT Input File	10
2a. Sample run_rec.track Standard Output File for Aircraft 1 Profile	18
2b. Sample run_rec.track Standard Output File for Aircraft 2 Profile	18
2c. Sample run_rec.track Standard Output File for Trial Results	18
2d. data1, data2, and data3 Interpretation	20
2e. Error Code Numbers Interpretation	20
3. Sample of AC_1.track Output File	20
4. Sample of AC_2.track Output File	21
5. Sample of RUN.track Output File	22
5. stats.stat Output File	24

1.0 SUMMARY

This document is a user manual for operating the PLAND_BLUNDER (PLB) simulation program. This simulation is based on two aircraft approaching parallel runways independently and using parallel Instrument Landing System (ILS) equipment during Instrument Meteorological Conditions (IMC). If an aircraft should deviate from its assigned localizer course toward the opposite runway, this constitutes a *blunder* which could endanger the aircraft on the adjacent path. The worst case scenario would be if the blundering aircraft were unable to recover and continue toward the adjacent runway. PLAND_BLUNDER is a Monte Carlo-type simulation which employs the events and aircraft positioning during such a *blunder situation*.

The model simulates two aircraft performing parallel ILS approaches using Instrument Flight Rules (IFR) or visual procedures. PLB uses a simple movement model and control law in three dimensions (X, Y, Z). The parameters of the simulation inputs and outputs are defined in this document along with a sample of the statistical analysis.

This document is the second volume of a two volume set. Volume 1 is a description of the application of the PLB to the analysis of close parallel runway operations.

2.0 INTRODUCTION

2.1 BACKGROUND

One of the major aviation problems in recent years has been the steady increase in the number and duration of flight delays. Airports have been unable to keep pace with traffic growth. A main component of these flight delays has been the capacity constraints placed on the current configuration of most airports. While this problem can best be solved by increasing airport capacity via constructing new airports and runways, few programs of this type are currently underway or even planned. With more efficient use of existing fixed airport resources, however, some modest changes in airport geometry can be made to better accommodate traffic. Therefore, during the past few years the FAA has initiated an airport capacity program designed to provide additional capacity at existing airports. Some of the improvements in this program include new Air Traffic Control (ATC) procedures, terminal automation, additional instrument landing systems, improved controller display aids, improved utilization of multiple runways, and improved airport and pavement design.

One of these improvements concerns parallel runway landings. Many airports have more than one runway to allow aircraft to land or depart from multiple runways. Controllers rely on the pilot's visual separation when runways are close together and weather conditions are good (i.e., as aircraft approach each other, the controller points out each aircraft to the pilot of the other aircraft and requires that the pilots maintain a safe spacing), and rely on radar to maintain a much larger spacing between aircraft when visibility is low (i.e., the pilots cannot be expected to maintain *safe spacing*). The capacity of an airport with multiple runways is less in IMC than in visual conditions. The amount of decreased capacity is dependent upon the spacing between runways.

Two controllers in the Terminal Approach Control Facility (TRACON) monitor traffic when conducting *simultaneous, independent parallel approaches* during instrument meteorological conditions. Each controller is assigned to monitor the traffic to one runway. The airspace between the runways is divided into three zones: the two Normal Operating Zones (NOZ) centered on the extended runway centerline representing the airspace needed to contain the normal approach tracks of all aircraft using the runway, and the No Transgression Zone (NTZ) in the middle representing the area that is normally kept free of aircraft. (Parallel runway approach zones are shown in *Figure 1*.)

Currently, the criterion is a separation of 4,300 ft or more between parallel runways for conducting independent instrument approaches. This standard was established based on the surveillance rate and accuracy of the Airport Surveillance Radars (ASR) and terminal Automated Radar Tracking System (ARTS) capabilities.

However, subsequent analysis has indicated that the separation between parallel runways could be reduced if the surveillance data rate and accuracy were improved. Surveillance and display technology are now available which should allow operations to be conducted on parallel runways separated by less than 4,300 ft.

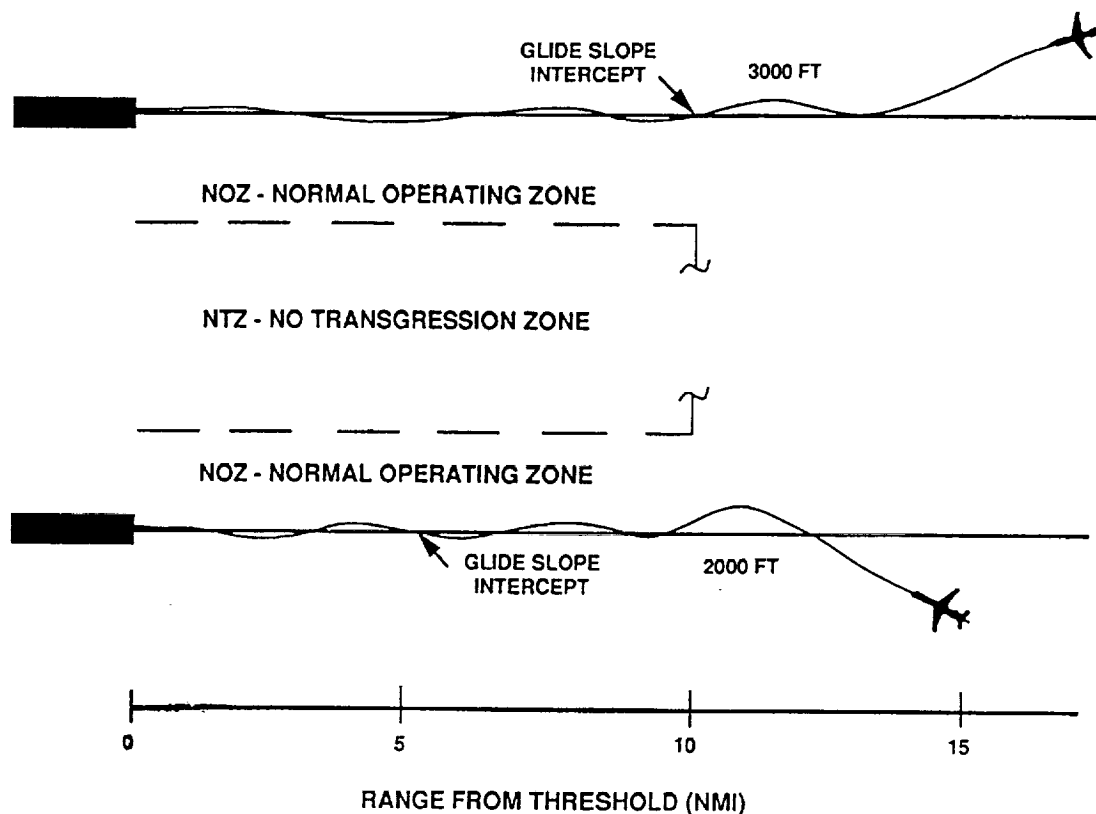


Figure 1. Parallel Runway Approach Zones

Present procedures provide 1,000 ft of vertical separation between aircraft during the time that the aircraft are turning onto and capturing the final approach course guidance. The aircraft normally maintain this vertical separation until intercepting the glideslope associated with their respective approach paths. Once the aircraft start their descent and the vertical separation is lost, the monitor controllers must assure that any penetration of the NTZ results in an appropriate control action to assure aircraft separation.

When runways are spaced between 2,500 ft and 4,300 ft apart, the controller must employ dependent parallel approach procedures which require that a spacing of at least 1.5 nm be maintained from aircraft approaching the adjacent runway. This spacing constraint means that an airport without the requisite spacing between runways suffers a capacity penalty of about 40% during IMC.

2.2 PRECISION RUNWAY MONITOR SYSTEM

Significant capacity gains can be achieved where closely spaced parallel runways exist by implementing the Precision Runway Monitor (PRM) system. This system consists of controller procedures and new equipment (i.e., radar and controller display). The PRM system is driven by an improved radar sensor. The PRM program is intended to improve runway acceptance and departure rates so that operations under instrument conditions more closely approximate those achievable in visual conditions.

The 4,300-foot separation standard (based on a 1981 Mitre Corporation requirement analysis) is the amount of time it might take an aircraft that has strayed from its approach course to traverse the area between the two parallel approach courses. Hence, the closer the runways and courses, the less time controllers have to rectify a potentially hazardous situation (i.e., termed a *blunder*). A blunder occurs when an aircraft begins to cross over toward the other approach course. A blunder can be rectified by the controllers first seeing it occur on the radar and then reacting to it by issuing an instruction to one or both aircraft. The pilots must then hear the instruction, and adjust the controls of the aircraft to respond. Finally, the aircraft itself must respond to the pilot's commands to get the aircraft heading away from the potential collision. When all these response times are added up, 20 to 30 sec can elapse between the beginning of a blunder (i.e., where two aircraft are beginning to converge) until the aircraft are redirected and begin to diverge.

The PRM program has been demonstrated at Memphis International and Raleigh-Durham airports (runway geometry shown in *Figure 2*) and designed to reduce two of these reaction times by three fold: the time it takes the radar to display a blunder, and the time it takes the controller to see it on the display and react to it. Conventional airport surveillance radars update the target position every 4 to 5 sec. If it is assumed that it takes two scans for the controller to detect a problem on a radar with a 5 sec update rate, then 10 sec will elapse before the controller issues an instruction to the pilot. If it is further assumed that a blundering aircraft moves toward the adjacent runway at 120 ft/sec, then that same 10 sec radar update delay could result in a loss of 1,200 ft. Put another way, each second of improvement in the update rate results in a reduction in allowable runway spacing of 240 ft.

Aside from the update rate, additional time can be saved with a more accurate radar and an improved controller display. Such refinements (i.e., the symbol portraying the aircraft on the display being smaller and the deviations from the on-course track being easier to recognize) will allow a controller to be certain of a blunder occurring and declare it earlier. Further computer processing of the track will allow for the generation of an automated alert which will lessen the reaction time of the controller.

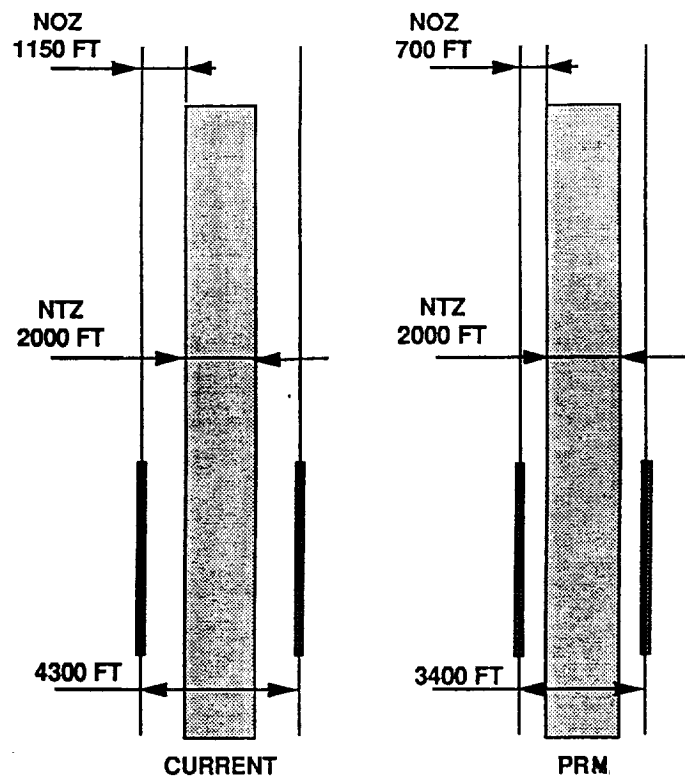


Figure 2. Normal Operating Zone Shrinks as Runway Separation is Reduced

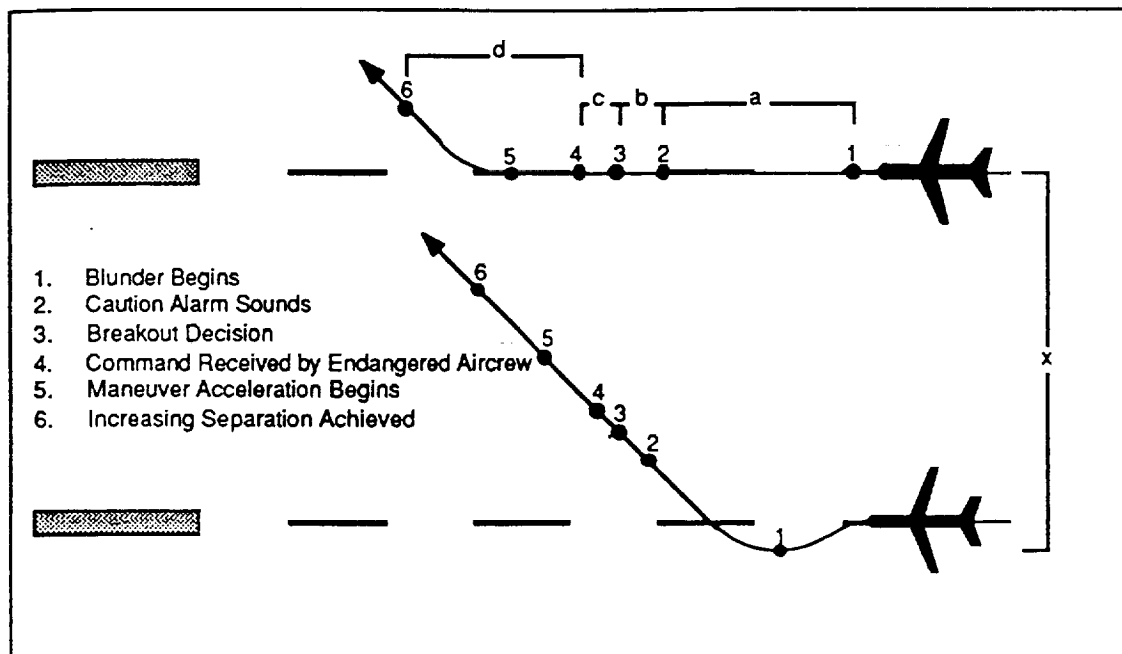


Figure 3. Blunder-Model Event Sequence

Furthermore, if a blunder should occur, then satisfactory resolution of that blunder requires that the evader aircraft be turned away in time to avoid a collision with the blundering aircraft. The amount of time available depends on several elements which characterize the performance of aircraft, air traffic control equipment, and their human operators. These elements can be understood from *Figure 3*, which shows a schematic diagram of a blunder. The elements are:

1. The time used by the sensor to detect the blunder and generate an alarm.
2. The time used by the monitor controller to recognize the alarm, decide whether a breakout instruction is needed, and determine when to issue the instruction.
3. The time required to communicate the instruction to the pilot of the endangered aircraft.
4. The time required for the aircraft crew to recognize the instruction and give the control inputs, and for the aircraft to respond to the control inputs and maneuver to the point where the separation between the aircraft is increasing.
5. The lateral distance between the two aircraft at the start of the blunder.

2.3 PLAND_BLUNDER SIMULATION PROGRAM

Two streams of aircraft approach the parallel runways independently of one another during independent parallel Instrument Landing System (ILS) approaches. If one aircraft deviates from its assigned localizer towards the opposite runways, there could be an endangered (evader) aircraft in its path. A deviation from the parallel approach towards the opposite runway constitutes a blunder. The worst case scenario would be for the blundering aircraft to be unable to recover (i.e., returning to the assigned approach) and continue toward the adjacent stream of aircraft. PLAND_BLUNDER (PLB) is a Monte Carlo-type fast simulation of the events and aircraft position during a worst case blunder situation. This model simulates two aircraft performing parallel ILS approaches using Instrument Flight Rules (IFR) or visual procedures with one aircraft blundering and the other possibly reacting to avoid the blunderer. PLB uses a very simple movement model and control law in three dimensions (X, Y, Z).

2.3.1 INPUT(S) OF SIMULATION PARAMETERS

The input parameters include: runway geometry, aircraft class, approach speed of aircraft, general type of blunder, general type of reaction, near miss criteria, and number of Monte Carlo cases to run. Some of the randomly influenced parameters are: initial along-track distance between aircraft, angle of blunder, location of

blunder, time to detect blunder, time to react by controller, time to react by pilot, aircraft response delay, and aircraft class.

2.3.2 ASSUMPTIONS AND LIMITATIONS

The movement model assumes the bank and pitch angles are decoupled and instantaneous. Turns are modeled as constant radius and level. There is no energy modeling of altitude, speed, and turning. The aircraft is assumed to follow the nominal profile plan with no minor adjustments to course, altitude and speed. There is no flight control system to react to perturbations or changes. The runways are assumed to be exactly parallel and level. Only the part of the approach after turn-on is modelled. The aircraft position update interval is .5 second. Each run is terminated 50 sec after the evasion maneuver starts, since it is assumed that the closest approach will have occurred before then. A blunder is considered to have occurred when either the alarm distance from the centerline or the edge of the NTZ is breached by the blundering aircraft. The alarm distance and the NTZ edge are set equal for IMC runs, whereas only the alarm distance defines a blunder for VMC runs.

2.3.3 OUTPUT OF SIMULATION

The standard output of PLB is the 1_run_single_line records file (run_rec.track). This describes each trial run as a one line summary of initial conditions and the results. Optional outputs are the tracks files (AC_1.track, AC_2.track and RUN_1.track). These track files record time-stamped data describing the movement of each aircraft in detail.

3.0 SYMBOLS AND ABBREVIATIONS

AC	Aircraft
ARTS	Automated Radar Tracking System
ASR	Airport Surveillance Radar
ATC	Air Traffic Control
FAA	Federal Aviation Administration
IFR	Instrument Flight Rules
ILS	Instrument Landing System
IMC	Instrument Meteorological Condition
NOZ	Normal Operating Zone
NTZ	No Transgression Zone
OS	Operating System
PLB	PLAND_BLUNDER Simulation Program
PRM	Precision Runway Monitor
RWY	Runway
SD	Standard Deviation
TAE	Total Azimuth Error
TRACON	Terminal Approach Control Facility
WP	Way Point

4.0 RUNNING THE PROGRAM

4.1 SOFTWARE INSTALLATION AND INFORMATION TO BUILD PLB SIMULATION

The main source files are *FORTRAN 77* with extension *.f* and employ files with extensions *.inc* and *.use*. All these files must be in the same working directory. The build scripts are for the *UNIX SYSTEM5 OS*.

To compile and link the simulation, type: **pland.blunder.make**

To compile and link the statistics, type: **pland.stat.make**

The simulation uses a random number generator. At Boeing this is available in library */tech/bin/bcslib* and the routines are called *HSRSUN* and *HSRSNR*. Outside Boeing these routines should be replaced by their equivalents. Changes should be made in *FORTRAN* file *random.f* and to the **pland.blunder.make** script.

4.2 INPUT FILES

The input file to the PLB simulation is in a command file: **pland_exec.dat**. *Table 1* shows a sample **pland_exec.dat** File.

4.2.1 OVERVIEW OF COMMANDS FOR THE PLB SIMULATION

A command interpreter extracts scenario definitions and run parameters from the commands.

Necessary definitions for a PLB simulation run are:

1. *Aircraft (AC) profiles 1 and 2* - Use a **AC_CASE** command for each aircraft.
2. *Aircraft (AC) types (1-6)* - Use a **AC_TYPE** command for each type used.
3. *Runway geometries 1 and 2* - Use a **RWY_DEF** command for each runway, or a **RWY_PAIR** command to define both.
4. *Number of trials run with same inputs* - Use a **RUN_X** command after other items are defined.
5. *QUIT command* - Use a **QUIT** command to signal the end of input.

Table 1. Sample PLAND_EXEC.DAT Input File

! Comment: Sample command file to show most capabilities without massive output data.

***** AC TYPE SEGMENT *****

! Comment: Define aircraft types and fleetmix.

```
AC_TYPE 4 SIZE 230.0 200.0 70.0 Tresponse 3.0 1.0 SPD 1,2 m+SD 170.0 10.0 140.0 5.0 kts
>>> ESC ACCEL,CLMB m+SD 30.0 10.0 40.0 10.0 TAE ANGLE(mR) m+SD -2.0 5.0
AC_TYPE 1 SIZE 50.0 60.0 30.0 Tresponse 2.0 1.0 SPD 1,2 m+SD 110.0 10.0 80.0 5.0 kts
>>> ESC ACCEL,CLMB m+SD 30.0 10.0 30.0 10.0 TAE ANGLE(mR) m+SD -3.0 10.0
AC_TYPE 2 SIZE 100.0 100.0 50.0 Tresponse 2.0 1.0 SPD 1,2 m+SD 140.0 10.0 110.0 5.0 kts
>>> ESC ACCEL,CLMB m+SD 30.0 10.0 40.0 10.0 TAE ANGLE(mR) m+SD -2.0 7.0
AC_TYPE 3 SIZE 150.0 160.0 60.0 Tresponse 3.0 1.0 SPD 1,2 m+SD 160.0 10.0 130.0 5.0 kts
>>> ESC ACCEL,CLMB m+SD 30.0 10.0 40.0 10.0 TAE ANGLE(mR) m+SD -2.0 5.0
FLEETMIX (1-6) 10.0 20.0 30.0 40.0 0.0 0.0
ALT_FMIK (1-6) 10.0 20.0 30.0 40.0 0.0 0.0
```

***** PROFILE SEGMENT *****

! Comment: Define the blunder and escape profiles for the aircraft.

```
AC CASE BLUNDER 1 AC 1 TYPE 0 RWY L Dstart 70000.0 Tstart m+SD 0.0 0.0
>>> dTURN 3.0 Dblund hi,lo 60761.0 60761.0 BLUND m+SD ANG 30.0 1.0 SLOPE 0.0 1.0 DV 0.0 10.0
AC CASE NORM_ESC 1 AC 2 TYPE 9 RWY R Dstart 70000.0 Tstart m+SD 0.0 0.0
>>> BANK m+SD 60.0 0.0 HEAD 50.0 CLIMB/ACCEL BY TYPE
```

***** RUNWAY GEOMETRY SEGMENT *****

! Comment: Define runway geometry.

```
RWY_DEF R THRESH 0.0 CENTERLINE,NOZ -2150.0 1150.0
RWY_DEF L THRESH 0.0 CENTERLINE,NOZ -2150.0 1150.0
```

***** RESPONSE TIME SEGMENT *****

! Comment: Define alarm criteria and response delay times..

```
ALARM Dalarm 300.0
RESPONSE SENSOR GAUSSIAN 3.0 1.0
RESPONSE ATC DISTR_FILE study.0.ATC.dat
RESPONSE COM GAUSSIAN 1.5 0.5
RESPONSE PILOT GAUSSIAN 4.0 1.0
```

***** RUNX SEGMENT *****

! Comment: Define the range of x-offset geometries and the number of runs.

```
STEP_T Tmin,max,step -3.0 3.0 2.0
RUN_X 3 SEED 7000000
QUIT
```


Optional definitions for PLB simulation run are:

1. *Delays for response times* - Use a DELAYS command to define response delay times. (Default is 0 delay.)
2. *Fleetmixes for random aircraft* - Use a FLEETMIX or ALT_MIX command.
3. *Offset time limits and step size* - Use a STEP_T command. (Default is using the Tstart data from the AC_CASE commands.)
4. *Single run tracks turned on* - Use a TRACKS command. (Default is no tracks files.)

4.2.1.1 DEFINITION OF COMMANDS AND PARAMETERS

The definitions of commands and parameters for the different commands are listed in *Appendix A* which can be used as a Reference Manual.

4.2.2. DESCRIPTION OF PROFILES

The final segment of the flight will be divided into two parts, distinguished by two different speeds for each aircraft, to create *Parallel ILS approach scenarios*. This will then support the PRM scenarios of approximately 10 and 2 miles from the runway threshold. For *dual parallel runway ILS approaches*, there are three possible aircraft profiles (i.e., AC-CASE):

1. NORMAL_1

(Example: AC_CASE NORMAL_1 AC 1 TYPE 4 RWY L Dstart 50000.00 Tstart m+SD 10.0 5.0)

NORMAL_1 follows a straight course down the runway centerline with touchdown at runway threshold. Aircraft type, runway assignment and speed for each Way-Points (WPs) are explicitly defined as:

Start to WP 1: glideslope = -3
speed = speed_1 (random) for this AC_TYPE

WP 1 to WP 2: glideslope = -3
speed = speed_2 (random) for this AC_TYPE

2. NORM_ESC_1

(Example: AC_CASE NORM_ESC_1 AC 2 TYPE 4 RWY R Dstart 70000.0 Tstart m+SD 0.0 0.0
BANK m+SD 60.0 0.0 HEAD 50.0 CLIMB/ACCEL BY TYPE)

NORM_ESC_1 follows the same course as NORMAL_1, until a collision avoidance command is given. The avoidance response is a turn away and climb. The aircraft type is explicitly defined as:

Start to WP 1: glideslope = -3
 speed = speed_1 (random) for this AC_TYPE

WP 1 to WP 2: glideslope is determined by type-dependent climb rate

where WP 2 is touchdown (speed = old_speed + type-dependent speed increase).

When the avoidance command is given the aircraft will turn away with BANK (random) until the course (HEAD) is established. Then the aircraft will straighten out and climb, and alter speed after the turn is completed.

3. BLUNDER_1

(Example: AC_CASE BLUNDER_1 AC 1 TYPE 3 RWY L Dstart 70000.0 Tstart m+SD
 0.0 0.0 dTURN 3.0 Dblunder hi, lo 60761.0 60761.0 BLUNDER m+SD ANG
 30.0 1.0 SLOPE 0.0 1.0 DV 0.0 10.)

BLUNDER_1 follows the same course as NORMAL_1 until the distance Dblunder (random) from the threshold is reached. The blunder can occur either before or after WP 1. The blunder is a change to a new heading and a new glideslope.

From start to WP 1: glideslope = -3
 WP 1 is blunder point speed = speed_1 (random) for this AC_TYPE

From WP 1 to WP 2: glideslope = specified glideslope (random)
 WP 2 is 10,000 ft
 past threshold speed = speed_2 (random) for this AC_TYPE

when blunder point reached: turn toward other runway with dTURN deg/sec
 till blunder-angle (random) reached, then
 straighten out and assume new glideslope
 (random), add DV to speed.

4.2.3 INTERPRETATION OF INPUT FILE

Each element comprising the Input File is defined here using *Table 1* as a reference.

4.2.3.1 AIRCRAFT TYPES AND FLEETMIX

AC_TYPE 4

AC_TYPE 4	Aircraft type definition for Type 4.
SIZE 230.0 200.0 70.0	Aircraft type dimension in ft: x = 230, y = 200, z = 60. (This type represents a Boeing 747 whose data is currently not being used by the simulation.)
Tresponse 3.0 1.0	Aircraft type time to respond to pilots control inputs, mean=3, standard deviation (SD) = 1 sec.
SPD 1, 2 m+SD 170.0 10.0 140.0 10.0	Aircraft type Speed1 and Speed2. Speed1 is faster, used further from runway, mean = 170, SD = 10 kn. Speed2 is slower, used closer to runway, mean = 140, and SD = 5 kn.
>>> ESC ACEL, CLMB m+SD 30.0 10.0 40.0 10.0	This is the second line of the AC_TYPE command defining the aircraft type, speed change and climb rate during collision avoidance maneuver. Speed change occurs instantaneously after the maneuver turn is complete. Speed change mean = 30 and SD = 10 fps. Climb rate is constant and applied after the maneuver turn is complete. Climb rate mean = 40 and SD = 10 fps.
TAE ANGLE (mR) m+SD -2.0 5.0	Aircraft offset or Total Azimuth Error (TAE) (flight technical error, radar error, etc.) crosstrack angle toward NTZ from runway centerline at threshold, mean=-2.0 and SD = 5.0 mR.

AC_TYPE 1, 2, 3

AC_TYPE 1, 2, 3 etc.	Aircraft type definition for Types 1, 2 and 3. The data follows the same format as for type 4. Types 5 and 6 are currently undefined and are available for expansion.
-------------------------------	---

FLEETMIX (1-6)

FLEETMIX (1-6)
10.0 20.0 30.0 40.0 0.0 0.0

Fleetmix aircraft type percentage definition for random aircraft types: aircraft Type 1 is 10%, Type 2 is 20%, Type 3 is 30%, type 4 is 40%, Types 5 and 6 are 0%, total is 100%.

ALT_FMDX (1-6)
0.0 0.0 30.0 20.0 30.0 20.0

Same definition as above (optionally one Fleetmix used for Blunderer and the other for evader).

4.2.3.2 RUNWAY GEOMETRY

RWY_DEF R

RWY_DEF R

Runway definition for right side runway.

THRESH 0.0

Threshold is at $x = 0$ and is not used.

CENTERLINE, NOZ 2150.0 1150.0

Runway centerline is at $y = 2150$ with NOZ extending 1,150 ft. on both sides.

RWY_DEF L

RWY_DEF L

Runway definition for left side runway.

THRESH 0.0

Threshold is at $x = 0$ and is not used.

CENTERLINE, NOZ -2150.0 1150.0

Runway centerline is at $y = -2150$ with NOZ extending 1,150 ft. on both sides.

Together these definitions define runway separation (rwy sep) = 4,300 ft and NTZ = 2,000 ft.

4.2.3.3 DEFINE ALARM CRITERIA

ALARM

Dalarm 300.0

The alarm criteria is 300 ft from extended runway centerline to start delay timers.

4.2.3.4 RESPONSE DELAY TIMES

RESPONSE DELAYS	Delay definitions with <i>delays</i> simulating response times for various systems.
RESPONSE SENSOR	This defines the sensor system response to initiate yellow alarm.
GAUSSIAN 3.0 1.0	This system has a <i>Gaussian</i> distribution for response time, with mean Delay =3.0 and SD=1.0 sec.
RESPONSE ATC	Controller time to interpret alarm and send instructions.
DISTR_FILE study_D.ATC.dat	This system's response time is defined by a cumulative distribution defined in file study_D.ATC.dat. The other option is, to define controller response time in the form of a <i>Gaussian</i> distribution with a mean and standard deviation.
RESPONSE COM	The ATC communication response time. A <i>Gaussian</i> distribution with a mean and standard deviation. The other option is, to define the communication response time in the form of a distribution.
PILOT 4.0 1.0	Pilot time to interpret instruction and move flight controls (mean delay = 4.0 sec. and SD= 1.0 sec). The other option is, to define the controller response time in the form of a <i>Gaussian</i> distribution with a mean and standard deviation.
AC_TYPE()	Comment reminding user that the aircraft type has a delay that's not set here

4.2.3.5 BLUNDER AND ESCAPE PROFILES FOR AIRCRAFT

AC_CASE

AC_CASE	Aircraft case or profile definition that defines general behavior of aircraft.
BLUNDER_1	Use BLUNDER_1 profile which turns to a constant blunder angle.
AC 1	This is for aircraft #1.
TYPE 0	Aircraft Type 0 indicates random type based on fleetmix percentages.
RWY L	Use left runway.
Dstart 70000.0	Start the simulated approach at 70,000 ft from the threshold.
Tstart m+SD 0.0 0.0	Start moving at time 0. This is over-ridden by STEP_T command.
>>> dTURN 3.0	Second line: The turn rate of the blunderer during the blunder is 3 deg/sec.
Dblund hi, lo 60761.0 60761.0	The blunder occurs 60,761 ft. (10 nm) from threshold.
BLUND m+SD ANG 30.0 10.0	Blunder angle which is the turn from course by the blunderer (mean = 30 and SD =1 deg).
SLOPE 0.0 1.0	Slope flown by blunderer after the blunder (mean = 0 and SD = 1 deg).
DV 0.0 10.0	Speed change by blunderer after the blunder (mean = 0 and SD = 10 fps).

AC_CASE

AC_CASE	Aircraft case or profile definition which defines the general behavior of aircraft.
NORM_ESC_1	Use NORM_ESC_1 profile to fly the approach normally until it gets a message to avoid blunderer, then it fly escape maneuver by turning to a given heading and climbing

AC 2	This is for Aircraft #2.
TYPE 3	Aircraft Type 3.
RWY R	Use right runway.
Dstart 70000.0	Start the simulated approach 70,000 ft from the threshold.
Tstart m+SD 0.0 0.0	Start moving at time 0. This is overridden by STEP_T command.
>>> BANK m+SD 60.0 0.0	Second line: Define escape maneuver bank angle (mean = 60 and SD = 0 deg).
HEAD 50.0	Define escape maneuver heading to 50 deg away from other runway.
CLIMB/ACCEL BY TYPE	This is a comment stating that the escape maneuver climb rate and speed change are based on aircraft type (3).

4.2.3.6 RANGE OF X-OFFSET GEOMETRIES AND NUMBER OF RUNS

STEP_T

STEP_T	Define iteration of trials varying time offsets. (Offset is between AC 1 and AC 2 start times in seconds.)
Tmin, max, step -3.0 3.0 2.0	Time offset steps from -3 to 3 sec at 2 sec intervals. (This could be set at -32 to 32 sec at 1 sec intervals, representing -1.5 to 1.5 nm at 287 fps.)

RUN-X

RUN_X 3	Define number of trials to run with the same time offsets. (This combined with the STEP-T will run $3 \times 4 = 12$ trials.)
SEED 7000000	Define initial random number seed.

QUIT

Quit	End of the simulation
------	-----------------------

4.3 RUNNING PBL SIMULATION

To run PLB simulation, type: `pland_exec.exe`. After entering this command the program will read the input file from `pland_exec.dat`. Then after the execution, the output will be stored under different files.

4.4 PLB SIMULATION OUTPUTS

The PLB simulation always creates a 1_run_single_line output file `run_rec.track`. Optionally, the simulation also creates *tracks* files showing time-stamped data for each run. The *tracks* files are turned on with the TRACKS command in the input file. These files can be extremely long for Monte-Carlo runs with large sample sizes. The *tracks* files are: `AC_1.track`, `AC_2.track`, and `RUN.track`.

The simulation also generates output in the shell output window. This output is not used for analysis, but is useful to verify the program is running.

4.4.1 run_rec.track OUTPUT FILE

The complete `run_rec.track` output file is listed in Table B1 of Appendix B. The header and the first two data lines are shown in Table 2(a-e).

Table 2a. Sample `run_rec.track` Standard Output File for Aircraft 1 Profile

PROFILE#1	RWY	TYPE	Dstrt#1	Tstrt#1	v1#1	v2#1	data1#1	data2#1	data3#1
BLUNDER_1	L	4	70000.0	3.0	293.0	225.5	293.0	30.3	1.1
BLUNDER_1	L	4	70000.0	3.0	297.2	234.9	297.2	30.7	-0.5

|-----aircraft 1 profile definition for this trial-----|

Table 2b. Sample `run_rec.track` Standard Output File for Aircraft 2 Profile

PROFILE#2	RWY	TYPE	Dstrt#2	Tstrt#2	v1#2	v2#2	data1#2	data2#2	data3#2
NORM_ESC_1	R	3	70000.0	0.0	260.0	198.7	60.0	47.4	288.3
NORM_ESC_1	R	3	70000.0	0.0	262.9	192.7	60.0	46.7	314.7

|-----aircraft 2 profile definition for this trial-----|

Table-2c. Sample `run_rec.track` Standard Output File for Trial Results

ERRCODE	AVOID	COLLIDE	Tresp	Dmiss	shad	Dmiss
0	T	F	15.5	536.7	1247.4	
0	T	F	20.2	2904.1	2904.1	

|-----trial results-----|

Each data line in *Table 2a-c* represents one simulation trial in which the parameters of the trial and results are summarized. Each aircraft profile is described as defined by the randomly drawn and nonrandom parameters for that trial. The data columns are defined as:

1. **PROFILE #1** - Aircraft 1 profile type name.
2. **RWY** - Aircraft 1 assigned runway.
3. **TYPE** - Aircraft 1 aircraft type.
4. **Dstrt #1** - Aircraft 1 starting distance from the runway threshold.
5. **Tstrt #1** - Aircraft 1 movement starting time.
6. **v1#1** - Aircraft 1 speed 1, the faster speed used further from the runway.
7. **v2#1** - Aircraft 1 speed 2, the slower speed used closer to the runway.
8. **data1#1** - Aircraft 1 profile-dependent data item 1 (see Table 2d for translation).
9. **data2#1** - Aircraft 1 profile-dependent data item 2 (see Table 2d for translation).
10. **data3#1** - Aircraft 1 profile-dependent data item 3 (see Table 2d for translation).
11. **PROFILE#2** - Aircraft 2 information given in the same format as for Aircraft 1.
12. **ERRCODE** - Simulation error code with 0 meaning no error (see Table 2e for translation).
13. **AVOID** - Flag set true if an avoidance maneuver was attempted.
14. **COLLIDE** - Flag set true if the two aircraft got within 500 feet of each other.
15. **Tresp** - Total response delay time from the aircraft violating the blunder criteria until the other aircraft starts its avoidance maneuver.
16. **Dmiss.shad** - Closest approach distance between the two aircraft when there is no evasion maneuver.
17. **Dmiss** - Closest approach distance between the two aircraft.

The key to interpreting the parts of the 1_run_single_line output file are in *Table 2* with the key to interpreting the **data1**, **data2**, and **data3** outputs being in *Table 2d* and the key to interpreting the error code numbers (final code=prime multiplied) being in *Table 2e*.

Table 2d. data1, data2, and data3 Interpretation

PROFILE NAME	data1	data2	data3
BLUNDER_1	DISTblunder	ANGblunder	SLOPEblunder
NORMAL1	0.0	0.0	0.0
NORM_ESC_1	BANK	CLIMB	SPEED

Table 2e. Error Code Numbers Interpretation

ERROR NAME	CODE #
no errors or warnings	0
rand draw, blunder_angle < 0, blunder turns away	3
rand draw, DISTblunder < 0	5
rand draw, DISTblunder > DISTstart	7
rand draw, BANK < 0, escaping AC turns toward	11
rand draw, Tsensor < 0	13
rand draw, Tatc < 0	17
rand draw, Tresponse < 0	19
rand draw, Tpilot < 0	23

4.4.2 AC_1.track OUTPUT FILE

The **AC_1.track** output file describes the state of Aircraft 1 after each timestep of the trial. Each data line describes one timestep. (Note: The complete output file **AC_1.track** has been listed in *Table B2* in *Appendix B*.) The header and the first two data lines are shown in *Table 3*.

Table 3. Sample of AC_1.track Output File

TI	RWY_lisL	X1	Y1	Z1	LEG1	HEAD1	V1	BANK1	SLOPE1
1.0	1	-70000.0	-2150.0	3668.5	1	0.0	293.0	0.0	-3.0
2.0	1	-70000.0	-2150.0	3668.5	1	0.0	293.0	0.0	-3.0

The data columns in *Table 3* are defined as:

1. **T1** - Time after simulation trial start (in seconds).
2. **RWY_1isL** - Runway assignment (where 1 is L and 2 is R).
3. **X1** - X location (in feet).
4. **Y1** - Y location (in feet).
5. **Z1** - Z location (in feet).
6. **LEG1** - Current waypoint leg (where LEG1 = 1 means heading toward the first waypoint).
7. **HEAD 1** - Heading (in degrees clockwise from runway centerline).
8. **V1** - Speed/total 3D ground speed (in ft/sec).
9. **BANK1** - Bank angle (in degrees right).
10. **SLOPE 1** - Glide slope (in degrees up).

4.4.3 AC_2.track OUTPUT FILE

The **AC_2.track** file describes the state of Aircraft 2 after each timestep of the trial with the headers and data columns of the file being analogous to those of the **AC_1.track** output file. (Note: The complete output file **AC_2.track** has been listed in *Table B3* of *Appendix B*.) The header and the first two data lines are shown in *Table 4*.

Table 4. Sample of AC_2.track Output File

T2	TWY_2isR	X2	Y2	Z2	LEG2	HEAD2	V2	BANK2	SLOPE2
1.0	2	-69740.0	2150.0	3654.9	1	0.0	260.0	0.0	-3.0
2.0	2	-69479.9	2150.0	3641.3	1	0.0	260.0	0.0	-3.0

4.4.4 RUN.track OUTPUT FILE

The **Run.track** output file describes the relationship between the two aircraft after each timestep of the trial with each data line describing one timestep. (Note: The complete **RUN.track** output file is listed in *Table B4* of *Appendix B*.) The header and the first two data lines are shown in *Table 5*.

Table 5. Sample of *RUN.track* Output File

TO	DISTshad	DISTshad_MIN	DIST	DIST_MIN	CLOSING_RATE
0.5	5308.0	5308.0	5308.0	5308.0	26.1
1.0	5295.0	5295.0	5295.0	5295.0	25.9

The data columns are defined as:

1. **TO** - Current time (in seconds).
2. **DIST** - Distance between AC 1 and AC 2 (in feet).
3. **DIST_MIN** - Minimum DIST so far in this trial (in feet).
4. **CLOSING_RATE** - Rate of change in distance between AC 1 and AC 2 (in ft/sec).

4.5 ANALYSIS OF DATA OUTPUT

After generating output files, the data can be analyzed and interpreted. The statistics programs used here is called **STATS**. Figure 4 shows the flow diagram of **PLB** program from setting up the input file to statistical analysis and plotting of the output data.

4.5.1 STATISTICAL ANALYSIS OF OUTPUT DATA

The statistics counting program **STATS** describes the distribution of miss-distances of the Monte-Carlo simulation trials. **STATS** reads the 1-run-per-line output file **run_rec.track** and counts each miss distance, putting each trial into a bin based on miss distance. The output is designed to be read by a plotting packaging. Several lines of the header are instructions to the **BOEING PEGASUS** plot package and can be removed or ignored. The output file is **stats.stat**. with output columns of:

1. **LO** - Lower bound of bin/miss distance (in feet).
2. **HI** - Upper bound of bin/miss distance (in feet).
3. **HITSper** - Proportion of trials with miss distance in this bin.
4. **HITSn** - Number of trials with miss distance in this bin.

5. **HITS_{per}_cum** - Proportion of trials with miss distance in this bin or less.

6. **HITS_n_cum** - Number of trials with miss distance in this bin or less.

A sample of a **stats.stat** output file is shown in *Table 6* with a plot of **stats.stat** presented in *Figure 5*.

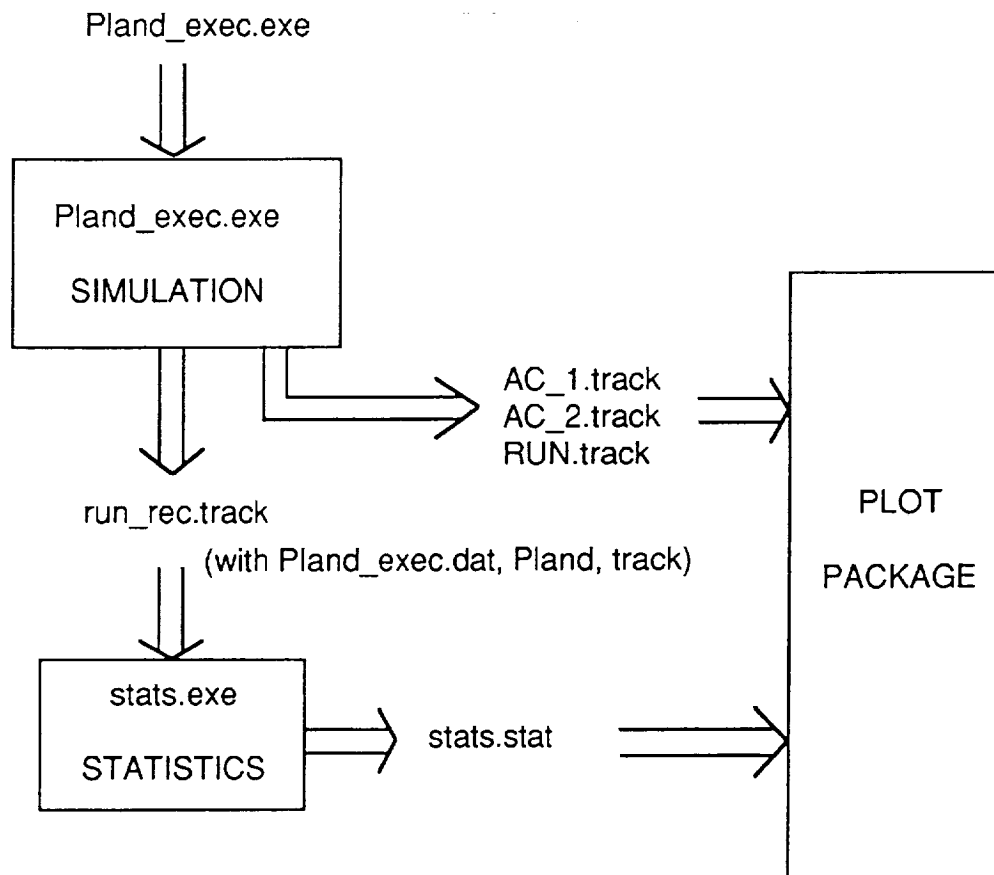


Figure 4. PBL Flow Diagram

Table 6. stats.stat Output File

RUNWAY SPACING OF 3400FT WITH 2000FT NTZ

```

! Comment: Define aircraft types and fleetmix.
! Comment: MITRE type : AC TYPE correlation (1:1 2:2 3:3 4:- 5:- 6:- 7:4 8:5 9:6)
AC TYPE 1 SIZE 100.0 100.0 50.0 Tresponse 0.0 0.0 SPD 1,2 m+SD 150.0 1.78 100.0 1.78 kts
>>> ESC ACCEL,CLMB m+SD 0.0 0.0 33.0 0.0 FTE ANGLE(mR) m+SD -1.0 3.0
AC TYPE 2 SIZE 100.0 100.0 50.0 Tresponse 0.0 0.0 SPD 1,2 m+SD 150.0 1.78 110.0 1.78 kts
>>> ESC ACCEL,CLMB m+SD 0.0 0.0 17.0 0.0 FTE ANGLE(mR) m+SD -1.0 3.0
AC TYPE 3 SIZE 100.0 100.0 50.0 Tresponse 0.0 0.0 SPD 1,2 m+SD 150.0 1.78 110.0 1.78 kts
>>> ESC ACCEL,CLMB m+SD 0.0 0.0 25.0 0.0 FTE ANGLE(mR) m+SD -1.0 3.0
AC TYPE 4 SIZE 230.0 200.0 70.0 Tresponse 0.0 0.0 SPD 1,2 m+SD 180.0 1.78 140.0 1.78 kts
>>> ESC ACCEL,CLMB m+SD 0.0 0.0 33.0 0.0 FTE ANGLE(mR) m+SD -1.0 3.0
AC TYPE 5 SIZE 230.0 200.0 70.0 Tresponse 0.0 0.0 SPD 1,2 m+SD 180.0 1.78 140.0 1.78 kts
>>> ESC ACCEL,CLMB m+SD 0.0 0.0 42.0 0.0 FTE ANGLE(mR) m+SD -1.0 3.0
AC TYPE 6 SIZE 230.0 200.0 70.0 Tresponse 0.0 0.0 SPD 1,2 m+SD 180.0 1.78 140.0 1.78 kts
>>> ESC ACCEL,CLMB m+SD 0.0 0.0 50.0 0.0 FTE ANGLE(mR) m+SD -1.0 3.0
FLEETMIX (1-6) 9.0 5.7 5.3 21.0 43.0 16.0

! Comment: Define the blunder and escape profiles for the aircraft.
AC CASE BLUNDER 1 AC 1 TYPE 0 RWY L Dstart 65000.0 Tstart m+SD 0.0 0.0
>>> dTURN 3.0 Dblund hi,lo 60761.0 60000.0 BLUND m+SD ANG 30.0 0.0 SLOPE -3.0 0.0 DV 0.0 0.0
AC CASE NORM_ESC 1 AC 2 TYPE 0 RWY R Dstart 65000.0 Tstart m+SD 0.0 0.0
>>> BANK m+SD 22.0 0.0 HEAD 55.0 CLIMB/ACCEL BY TYPE

! Comment: Define runway geometry.
RWY_PAIR SEP 3400.0 NTZ 2000.0

! Comment: Define alarm criteria and response delay times
ALARM Dalarm 340.0

RESPONSE SENSOR GAUSSIAN 5.0 5.0
RESPONSE ATC GAUSSIAN 0.0 0.0
RESPONSE COM GAUSSIAN 0.0 0.0
RESPONSE PILOT GAUSSIAN 0.0 0.0

! Comment: Define the range of x-offset geometries and the number of runs.
! Comment: Evader ranges from 2500 ahead to 3500 feet behind blunderer.
STEP DX DXmin,max,step -2500.0 3500.0 250.0
RUN X 4 SEED 9876543
QUIT

```

```

*ESA
run1
*FLOAT
LO HI HITSper HITSn HITSper_cum HITSn_cum
0.0 100.0 0.0000 0 0.0000 0
100.0 200.0 0.0000 0 0.0000 0
200.0 300.0 0.0100 1 0.0100 1
300.0 400.0 0.0100 1 0.0200 2
400.0 500.0 0.0200 2 0.0400 4
500.0 600.0 0.0000 0 0.0400 4
600.0 700.0 0.0100 1 0.0500 5
700.0 800.0 0.0000 0 0.0500 5
800.0 900.0 0.0300 3 0.0800 8
900.0 1000.0 0.0000 0 0.0800 8
1000.0 1100.0 0.0100 1 0.0900 9
1100.0 1200.0 0.0100 1 0.1000 10
1200.0 1300.0 0.0400 4 0.1400 14
1300.0 1400.0 0.0100 1 0.1500 15
1400.0 1500.0 0.0100 1 0.1600 16
1500.0 1600.0 0.0500 5 0.2100 21
1600.0 1700.0 0.0600 6 0.2700 27
1700.0 1800.0 0.0400 4 0.3100 31
1800.0 1900.0 0.0300 3 0.3400 34
1900.0 2000.0 0.0200 2 0.3600 36
2000.0 2100.0 0.0600 6 0.4200 42
2100.0 2200.0 0.0300 3 0.4500 45
2200.0 2300.0 0.0800 8 0.5300 53
2300.0 2400.0 0.0200 2 0.5500 55
2400.0 2500.0 0.0600 6 0.6100 61

```

Table 6. stats.stat Output File (Concluded)

2500.0	2600.0	0.0400	4	0.6500	65
2600.0	2700.0	0.0400	4	0.6900	69
2700.0	2800.0	0.0500	5	0.7400	74
2800.0	2900.0	0.0100	1	0.7500	75
2900.0	3000.0	0.0300	3	0.7800	78
3000.0	3100.0	0.0400	4	0.8200	82
3100.0	3200.0	0.0100	1	0.8300	83
3200.0	3300.0	0.0300	3	0.8600	86
3300.0	3400.0	0.0400	4	0.9000	90
3400.0	3500.0	0.0000	0	0.9000	90
3500.0	3600.0	0.0200	2	0.9200	92
3600.0	3700.0	0.0100	1	0.9300	93
3700.0	3800.0	0.0000	0	0.9300	93
3800.0	3900.0	0.0200	2	0.9500	95
3900.0	4000.0	0.0000	0	0.9500	95
4000.0	4100.0	0.0000	0	0.9500	95
4100.0	4200.0	0.0100	1	0.9600	96
4200.0	4300.0	0.0000	0	0.9600	96
4300.0	4400.0	0.0100	1	0.9700	97
4400.0	4500.0	0.0100	1	0.9800	98
4500.0	4600.0	0.0100	1	0.9900	99
4600.0	4700.0	0.0100	1	1.0000	100
4700.0	4800.0	0.0000	0	1.0000	100
4800.0	4900.0	0.0000	0	1.0000	100
4900.0	5000.0	0.0000	0	1.0000	100
5000.0	5100.0	0.0000	0	1.0000	100
5100.0	5200.0	0.0000	0	1.0000	100
5200.0	5300.0	0.0000	0	1.0000	100
5300.0	5400.0	0.0000	0	1.0000	100
5400.0	5500.0	0.0000	0	1.0000	100
5500.0	5600.0	0.0000	0	1.0000	100
5600.0	5700.0	0.0000	0	1.0000	100
5700.0	5800.0	0.0000	0	1.0000	100
5800.0	5900.0	0.0000	0	1.0000	100
5900.0	6000.0	0.0000	0	1.0000	100
6000.0	6100.0	0.0000	0	1.0000	100
6100.0	6200.0	0.0000	0	1.0000	100
6200.0	6300.0	0.0000	0	1.0000	100
6300.0	6400.0	0.0000	0	1.0000	100
6400.0	6500.0	0.0000	0	1.0000	100
6500.0	6600.0	0.0000	0	1.0000	100
6600.0	6700.0	0.0000	0	1.0000	100
6700.0	6800.0	0.0000	0	1.0000	100
6800.0	6900.0	0.0000	0	1.0000	100
6900.0	7000.0	0.0000	0	1.0000	100
7000.0	7100.0	0.0000	0	1.0000	100
7100.0	7200.0	0.0000	0	1.0000	100
7200.0	7300.0	0.0000	0	1.0000	100
7300.0	7400.0	0.0000	0	1.0000	100
7400.0	7500.0	0.0000	0	1.0000	100
7500.0	7600.0	0.0000	0	1.0000	100
7600.0	7700.0	0.0000	0	1.0000	100
7700.0	7800.0	0.0000	0	1.0000	100
7800.0	7900.0	0.0000	0	1.0000	100
7900.0	8000.0	0.0000	0	1.0000	100
8000.0	8100.0	0.0000	0	1.0000	100
8100.0	8200.0	0.0000	0	1.0000	100
8200.0	8300.0	0.0000	0	1.0000	100
8300.0	8400.0	0.0000	0	1.0000	100
8400.0	8500.0	0.0000	0	1.0000	100
8500.0	8600.0	0.0000	0	1.0000	100
8600.0	8700.0	0.0000	0	1.0000	100
8700.0	8800.0	0.0000	0	1.0000	100
8800.0	8900.0	0.0000	0	1.0000	100
8900.0	9000.0	0.0000	0	1.0000	100
9000.0	9100.0	0.0000	0	1.0000	100
9100.0	9200.0	0.0000	0	1.0000	100
9200.0	9300.0	0.0000	0	1.0000	100
9300.0	9400.0	0.0000	0	1.0000	100
9400.0	9500.0	0.0000	0	1.0000	100
9500.0	9600.0	0.0000	0	1.0000	100
9600.0	9700.0	0.0000	0	1.0000	100
9700.0	9800.0	0.0000	0	1.0000	100
9800.0	9900.0	0.0000	0	1.0000	100
9900.0	10000.0	0.0000	0	1.0000	100
10000.0	99999.9	0.0000	0	1.0000	100
*EOD					
TOTALn=		100			

RUNWAY SPACING OF 3400FT WITH 2.4 UPDATE RATE

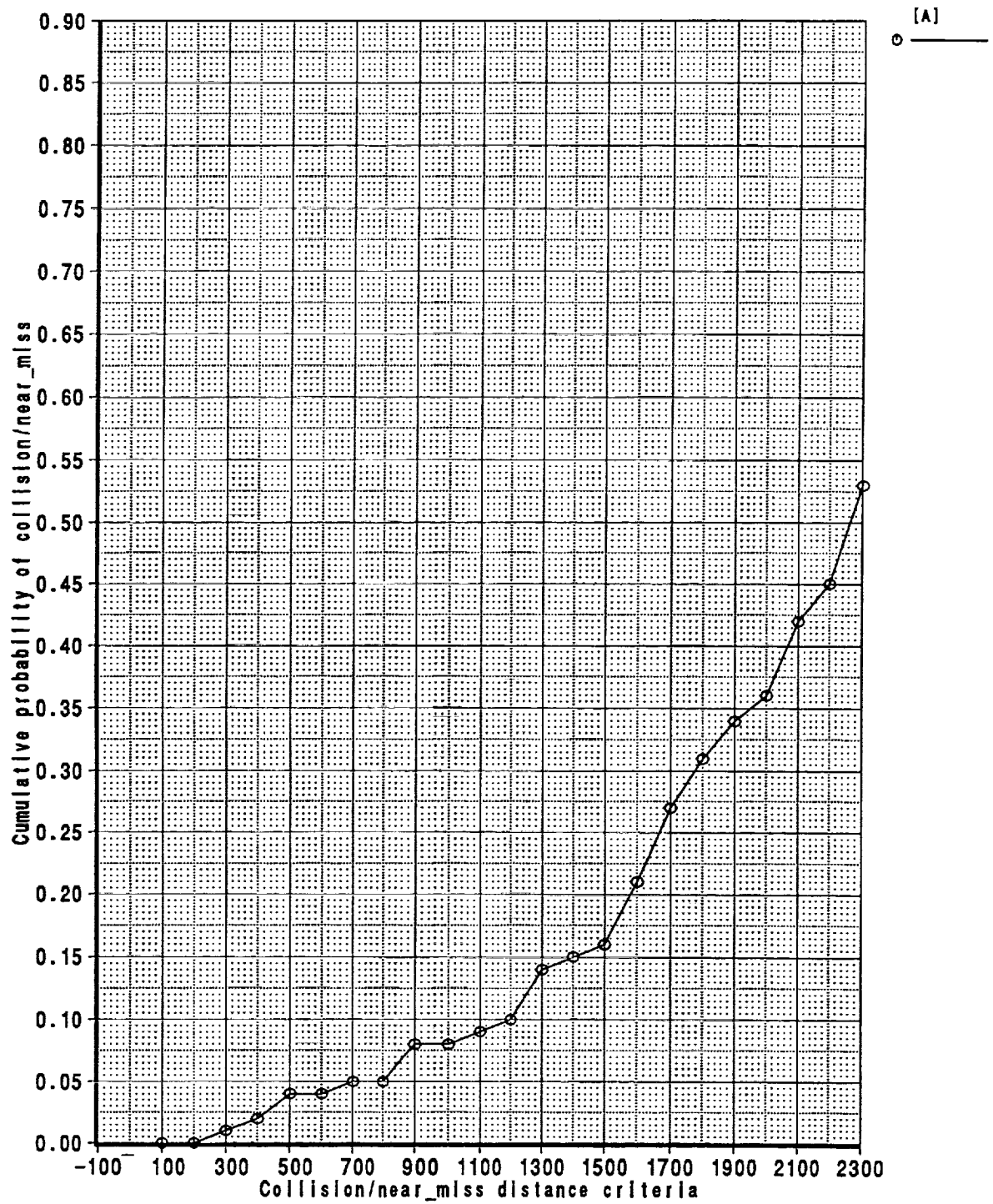


Figure 5. Plot of stats.stat

APPENDIX A
REFERENCE MANUAL

INFORMATION TO BUILD PLAND_BLUNDER SIMULATION

The main source files are FORTRAN 77 with extension .f.
They use include files with extensions .inc and .use.
All these files must be in the same working directory.
The build scripts are for the UNIX SYSTEM5 OS.

To compile and link the simulation type: pland.blunder.make
To compile and link the statistics type: pland.stat.make

The simulation uses a random number generator. At Boeing this is available in library /tech/bin/bcslib and the routines are called HRSR SUN and HRSR NR. Outside Boeing these routines should be replaced by their equivalents. Changes should be made in FORTRAN file random.f and to the pland.blunder.make script.

INFORMATION TO RUN PLAND_BLUNDER SIMULATION

To run PLAND_BLUNDER simulation, type: pland_exec.exe
The input is in file pland_exec.dat
The output is in file run_rec.track,
optional outputs are files AC_1.track, AC_2.track, RUN_1.track.

To run the statistics counter, type: stats.exe
The input is file run_rec.track,
The output is file stats.stat

In a study, it may be desirable to examine only a subrange of possible initial along-track offset positions. The STEP_T and STEP_DX commands are designed to control the along-track offset positions (via relative start-time or start_distance). The statistics program bases its percentages on only the cases actually run, even though the cases not run probably didn't get close to a collision. The statistics program STATS.F contains a factor STEPFAC TOR, which can be set to multiply times the percentages, to account for the cases not run.

OVERVIEW OF COMMANDS FOR THE PLAND_BLUNDER SIMULATION

The input to the PLAND_BLUNDER simulation is in a command file 'pland_exec.dat'.
A command interpreter extracts scenario definitions and run parameters from the commands.

Necessary definitions for a PLAND_BLUNDER sim run are:

Aircraft profiles 1 & 2 : use a AC_CASE cmd for each aircraft.
Aircraft types : use a AC_TYPE cmd for each type used.
Runway geometries 1 & 2 : use a RWY_DEF cmd for each runway,
or a RWY_PAIR cmd to define both.
Alarm criteria : use a ALARM cmd to define alarm criteria
trials run with same inputs : use a RUN_X cmd after other items are defined.
QUIT command : use a QUIT cmd to signal the end of input.

Optional definitions are :

Delays for response times : use a RESPONSE cmd. Default is 0 delay time.
Fleetsmixes for random aircraft: use a FLEETMIX or ALT_FMIX cmd.
Offset time/dist limits & : use a STEP_T cmd. Default is the AC_CASE Tstart data.
stepsize or a STEP_DX cmd. Default is the AC_CASE Dstart data.
Single run tracks turned on : use a TRACKS cmd. Default is no tracks files.

SAMPLE pland_exec.dat FILE

! Comment: Turn on detailed tracks files
TRACKS

! Comment: Define aircraft types and fleetsmix.

```
AC_TYPE 1 SIZE 50.0 60.0 30.0 Tresponse 2.0 1.0 SPD 1,2 m+SD 90.0 10.0 70.0 5.0
>>> ESC ACCEL,CLMB m+SD 30.0 10.0 30.0 10.0 TAE ANGLE(mR) m+SD -3.0 10.0
AC_TYPE 2 SIZE 100.0 100.0 50.0 Tresponse 2.0 1.0 SPD 1,2 m+SD 140.0 10.0 100.0 5.0
>>> ESC ACCEL,CLMB m+SD 30.0 10.0 40.0 10.0 TAE ANGLE(mR) m+SD -2.0 7.0
AC_TYPE 3 SIZE 150.0 160.0 60.0 Tresponse 3.0 1.0 SPD 1,2 m+SD 160.0 10.0 130.0 10.0
>>> ESC ACCEL,CLMB m+SD 30.0 10.0 40.0 10.0 TAE ANGLE(mR) m+SD -2.0 5.0
AC_TYPE 4 SIZE 230.0 200.0 70.0 Tresponse 3.0 1.0 SPD 1,2 m+SD 170.0 10.0 140.0 10.0
>>> ESC ACCEL,CLMB m+SD 30.0 10.0 40.0 10.0 TAE ANGLE(mR) m+SD -2.0 5.0
FLEETMIX (1-6) 10.0 20.0 30.0 40.0 0.0 0.0
```

! Comment: Define runway geometry.
RWY_PAIR SEP 3400.0 NTZ 2000.0

! Comment: Define alarm criteria and response delay times.

```
ALARM Dalarm 300.0
RESPONSE SENSOR GAUSSIAN 3.0 1.0
RESPONSE ATC DISTR FILE PRM_proto.ATC.dat
RESPONSE PILOT GAUSSIAN 4.0 1.0
```

! Comment: Define the blunder and escape profiles for the aircraft.

```
AC_CASE BLUNDER_1 AC 1 TYPE 0 RWY L Dstart 70000.0 Tstart m+SD 0.0 0.0
>>> dTURN 3.0 Dblund hi,lo 10001.0 9000.0 BLUND m+SD ANG 30.0 1.0 SLOPE 0.0 1.0 DV 0.0 5.0
AC_CASE NORM_ESC_1 AC 2 TYPE 3 RWY R Dstart 70000.0 Tstart m+SD 0.0 0.0
>>> BANK m+SD 60.0 0.0 HEAD 50.0 CLIMB/ACCEL BY TYPE
```

! Comment: Define the range of x-offset geometries and the number of steps.

```
! Commented out: STEP_T Tmin,max,step -3.0 3.0 2.0
STEP_DX DXmin,max,step -8000.0 8000.0 1000.0
```

! Comment: The commands above are order-independent.

! Comment: The commands below must be last and in that order.

```
RUN_X 3 SEED 7000000
QUIT
```

off

DEFINITION OF COMMANDS

TRACKS -- Turn on single-run time-stamped tracks output.
RWY_DEF -- Define 1 runway.
RWY_PAIR -- Define a pair of parallel runways.
RESPONSE -- Define the delay times describing a systems' response to a blunder.
ALARM -- Define the condition when a blunder alarm is triggered.
AC_TYPE -- Define the attributes specific to a class or type of aircraft.
FLEETMIX -- Define % of each aircraft type for the main fleetmix (TYPE 0 in AC_CASE).
ALT_FMIX -- Define % of each aircraft type for the alternate fleetmix (TYPE 9 in AC_CASE).
AC_CASE -- Define 1 aircrafts case profile.
STEP_T -- Define a series of runs iterating over a range of offset times tween the 2 AC.
STEP_DX -- Define a series of runs iterating over a range of offset dists tween the 2 AC.
RUN_X -- Run the monte-carlo simulation, and define the iteration parameters.
QUIT -- Quit the simulation, no more data.
other -- Any lines that don't start with one of the above commands are comment lines.

DEFINITION OF PARAMETERS FOR AC_CASE COMMAND

AC_CASE -- Aircraft profile type (NORMAL_1, BLUNDER_1, NORM_ESC_1),
-- general description of 1 aircrafts flight,
AC -- Aircraft ID (1-2)
TYPE -- Aircraft type or class number (1-6). Refers to AC_TYPE definition.
-- Type 0 uses main random fleetmix, type 9 uses alternate random fleetmix.
RWY -- Runway aircraft is to land on (L-R). Refers to RWY_DEF definition.
Dstart -- Distance from the runway threshold that the simulated aircraft starts at.
Tstart m+SD -- Time that the simulated aircraft starts moving.

(FOR normal_1 PROFILE)

no additional parameters

example:

AC_CASE normal_1 AC 2 RWY L DISTstart 50000.0

(FOR blunder_1 PROFILE, additional parameters on the 2nd line)

dTURN -- Turn rate of the aircraft during the blunder turn, in deg/sec.
Dblund -- Distance from the runway threshold that the aircraft blunders at,
hi,lo defined by a maximum and minimum distance in feet.
BLUND m+SD
ANG -- Blunder angle mean and standard deviation.
SLOPE -- Glideslope followed after the blunder, mean & std.dev. in deg, + is up.
DV -- Speed change made at the start of the blunder, mean & std.dev. in fps.

example:

AC_CASE BLUNDER_1 AC 1 TYPE 3 RWY L Dstart 70000.0 Tstart m+SD 0.0 0.0
>>> dTURN 3.0 Dblund hi,lo 60761.0 9000.0 BLUND m+SD ANG 30.0 1.0 SLOPE 0.0 1.0 DV 0.0 5.0

(FOR norm_esc 1 PROFILE, additional parameters on the 2nd line)

BANK m+SD -- Bank angle during the escape maneuver, mean & std.dev, deg.
HEAD -- Heading to be turned towards during the escape maneuver, deg.

example:

AC_CASE NORM_ESC_1 AC 2 TYPE 4 RWY R Dstart 70000.0 Tstart m+SD 0.0 0.0
>>> BANK m+SD 60.0 0.0 HEAD 50.0 CLIMB/ACCEL BY TYPE

DEFINITION OF PARAMETERS FOR AC_TYPE COMMAND

AC_TYPE -- Aircraft type or class number, 1-6.
SIZE -- Aircraft XYZ dimensions in feet.
Tresponse -- Aircraft time to respond to controls, mean & std.dev. in secs.
SPD -- Aircraft speeds, higher spd mean & std.dev, lower spd mean & std.dev, kts.
--(The following parameters are on the 2nd line of the AC_TYPE command)
>>> ESC ACEL -- Aircraft speed increase at start of escape maneuver, mean & std.dev, fps.
CLMB m+SD -- Aircraft climb rate during escape maneuver, mean & std.dev, fps.
TAE ANGLE(mR) -- Aircraft total azimuth err (TAE) crosstrack angle toward NTZ
-- from rwy centerline at threshold, mean & std.dev, milliradians.

example:

AC_TYPE 4 SIZE 150.0 160.0 60.0 Tresponse 2.0 1.0 SPD 1,2 m+SD 170.0 10.0 140.0 10.0
>>> ESC ACEL,CLMB m+SD 20.0 5.0 30.0 10.0 TAE ANGLE(mR) m+SD -1.0 3.0

DEFINITION OF PARAMETERS FOR FLEETMIX OR ALT_FMIX COMMANDS

FLEETMIX (1-6) -- Percentages of each aircraft type of the total fleetmix.
Aircraft_type 1 is first, type_6 is last, total must=100%.

examples:

FLEETMIX (1-6) 10.0 20.0 30.0 20.0 0.0 20.0
ALT_FMIX (1-6) 0.0 0.0 30.0 20.0 30.0 20.0

DEFINITION OF PARAMETERS FOR RWY_DEF COMMAND

RWY_DEF -- Runway being defined (L-R)
 THRESH -- Threshold, not yet implemented
 CENTERLINE,NOZ -- Runway centerline y, normal-operating-zone distance from centerline
 Assumes runway centerline and NOZ parallel to other runway.
 example:
 RWY_DEF R THRESH 100.0 CENTERLINE,NOZ -2000.0 1000.0

DEFINITION OF PARAMETERS FOR RWY_PAIR COMMAND

SEP -- Separation between the 2 parallel runway centerlines, in ft.
 NTZ -- Width of the No-Transgression-Zone in ft. The NTZ is assumed to be
 located symmetrically between the runways.
 example:
 RWY_PAIR SEP 3400.0 NTZ 2000.0

DEFINITION OF PARAMETERS FOR ALARM COMMAND

Dalarm -- Distance from the rwy centerline to trigger the alarm, feet.
 -- Also, if the aircraft enters the NTZ then the alarm will trigger.
 example:
 ALARM Dalarm 300.0

DEFINITION OF PARAMETERS FOR RESPONSE COMMAND

SENSOR -- Which system response is being defined. (SENSOR or ATC or COM or PILOT)
 GAUSSIAN -- Type of response time distribution (GAUSSIAN or DISTR_FILE)
 (FOR GAUSSIAN RESPONSE)
 -- GAUSSIAN is followed by the mean and std.dev in secs.
 example:
 RESPONSE SENSOR GAUSSIAN 3.0 1.0
 (FOR DISTR_FILE RESPONSE)
 -- DISTR_FILE is followed by the name of the file defining the distribution.
 example:
 RESPONSE ATC DISTR_FILE PRM_proto.ATC.dat

The DISTR_FILE describes the cumulative distribution of the response times.
 The file must have 1 line for each time/probability point, with time 1st and prob. 2nd.
 The probability is the proportion of trials when the response occurs at or before the time.
 Response time can be negative, indicating prediction.

DEFINITION OF PARAMETERS FOR STEP_T COMMAND

Tmin -- Minimum offset time for AC_2 to follow AC_1 by, secs.
 Tmax -- Maximum offset time for AC_2 to follow AC_1 by, secs.
 Tstep -- Stepsize to vary offset time by, secs.
 example:
 STEP_T Tmin,max,step -100.0 100.0 20.0

DEFINITION OF PARAMETERS FOR STEP_DX COMMAND

DXmin -- Minimum offset distance for AC_2 to follow AC_1 by, feet.
 DXmax -- Maximum offset distance for AC_2 to follow AC_1 by, feet.
 DXstep -- Stepsize to vary offset distance by, feet.
 example:
 STEP_DX DXmin,max,step -6000.0 6000.0 2000.0

DEFINITION OF PARAMETERS FOR RUN_X COMMAND

RUN_X -- Number of monte-carlo runs to make.
 SEED -- Random number generator seed.
 example:
 RUN_X 1 SEED 2000000

COMMAND FORMATS AND EXAMPLES

Each line of each command is presented as 3 lines:

EXAMPLE
BLANK FORM
FORMAT

FLIGHT PROFILE (3 variants, NORM_ESC_1 and BLUNDER_1 variants need 2 lines each)

```
AC CASE NORMAL 1 AC 1 TYPE 4 RWY L Dstart 50000.0 Tstart m+SD 10.0 5.0
AC CASE NORMAL 1 AC TYPE RWY Dstart Tstart m+SD
22xxxxxxxxxxxxxxxxxxxxx17xxxxxx16xxxxxa9xxxxxxxx9ffffff13xxxxxxxxxx6fffff6fffff

AC CASE NORM_ESC_1 AC 2 TYPE 3 RWY R Dstart 70000.0 Tstart m+SD 0.0 0.0
AC CASE NORM_ESC_1 AC TYPE RWY Dstart Tstart m+SD
22xxxxxxxxxxxxxxxxxxxxx17xxxxxx16xxxxxa9xxxxxxxx9ffffff13xxxxxxxxxx6fffff6fffff
>>> BANK m+SD 60.0 0.0 HEAD 50.0 CLIMB/ACCEL BY TYPE
>>> BANK m+SD HEAD CLIMB/ACCEL BY TYPE
18xxxxxxxxxxxxxxxxxx5ffff5ffff6xxxxx5ffff

AC CASE BLUNDER 1 AC 1 TYPE 3 RWY L Dstart 70000.0 Tstart m+SD 0.0 0.0
AC CASE BLUNDER 1 AC TYPE RWY Dstart Tstart m+SD
22xxxxxxxxxxxxxxxxxxxxx17xxxxxx16xxxxxa9xxxxxxxx9ffffff13xxxxxxxxxx6fffff6fffff
>>> dTURN 3.0 Dblund hi,lo 60761.0 60761.0 BLUND m+SD ANG 30.0 1.0 SLOPE 0.0 1.0 DV 0.0 10.0
>>> dTURN Dblund hi,lo BLUND m+SD ANG SLOPE DV
14xxxxxxxxxxxx4ffff14xxxxxxxxxx8ffffff8ffffff16xxxxxxxxxxxxxx6fffff5ffff6xxxxx5ffff5ffff3xx5ffff5ffff
```

AC_TYPE DEFINITION (2 lines per command)

```
AC_TYPE 4 SIZE 150.0 160.0 60.0 Tresponse 2.0 1.0 SPD 1,2 m+SD 160.0 10.0 130.0 5.0
AC_TYPE SIZE Tresponse SPD 1,2 m+SD
8aaaaaaaa17xxxxxx6fffff6fffff6fffff10xxxxxxxx5ffff5ffff14xxxxxxxxxx6fffff5 fff6fffff5ffff
>>> ESC ACEL,CLMB m+SD 20.0 5.0 30.0 10.0 TAE ANGLE(mR) m+SD -1.0 3.0
>>> ESC ACEL,CLMB m+SD TAE ANGLE(mR) m+SD
27xxxxxxxxxxxxxxxxxxxxxx5ffff5ffff5ffff5ffff20xxxxxxxxxxxxxxxxxx6fffff6fffff
```

FLEETMIX DEFINITION (2 variants)

```
FLEETMIX (1-6) 10.0 20.0 30.0 20.0 0.0 20.0
FLEETMIX (1-6)
8aaaaaaaa8xxxxxx6fffff6fffff6fffff6fffff6fffff6fffff

ALT FMIX (1-6) 0.0 0.0 30.0 20.0 30.0 20.0
ALT FMIX (1-6)
8aaaaaaaa8xxxxxx6fffff6fffff6fffff6fffff6fffff6fffff
```

RUNWAY DEFINITION COMMAND (2 variants)

```
RWY_DEF R THRESH 100.0 CENTERLINE,NOZ -2000.0 1000.0
RWY_DEF THRESH CENTERLINE,NOZ
8aaaaaaaaa9xxxxxxxx9ffffff17xxxxxxxxxxxxxxxxxx8ffffffx8ffffff

RWY PAIR SEP 3400.0 NTZ 2000.0
RWY PAIR SEP NTZ
8aaaaaaaa6xxxxx7fffff5xxxx7fffff
```

ALARM DEFINITION COMMAND

```
ALARM Dalarm 650.0
ALARM Dalarm
16xxxxxxxxxxxxxxxx7fffff
```

RESPONSE DELAY TIME DEFINITION COMMAND (2 variants)

```
RESPONSE SENSOR GAUSSIAN 30.0 10.0
RESPONSE GAUSSIAN
9xxxxxxxx6aaaaax10aaaaaaaaax5ffff5ffff

RESPONSE ATC DISTR_FILE PRM_proto.ATC.dat
RESPONSE DISTR_FILE
9xxxxxxxx6aaaaax10aaaaaaaaax28aaaaaaaaaaaaaaaaaaaaaaaaaaaa
```

TIME OFFSET ITERATION COMMAND

STEP T Tmin,max,step -100.0 100.0 20.0
 STEP T Tmin,max,step
 8aaaaaaa16xxxxxxxxxxxxxx7ffffff7ffffff7ffffff

DISTANCE OFFSET ITERATION COMMAND

STEP DX DXmin,max,step -10000.0 10000.0 1000.0
 STEP DX DXmin,max,step
 8aaaaaaa16xxxxxxxxxxxxxx9ffffff9ffffff9ffffff

MONTE-CARLO RUN COMMAND

RUN X 9 SEED 2000000
 RUN X SEED
 8aaaaaaax5iiii9xxxxxxxx10iiiiiii

APPENDIX B

OUTPUT FILES

TABLE B1.-run_rec.track Output File

PROFILE#1	RMY TYPE	DATA#1	DATA#2	DATA#3	DATA#4	DATA#5	DATA#6	DATA#7	DATA#8	DATA#9	DATA#10	DATA#11	DATA#12	DATA#13	DATA#14	DATA#15	DATA#16	DATA#17	DATA#18	DATA#19	DATA#20	DATA#21	DATA#22	DATA#23	DATA#24	DATA#25	DATA#26	DATA#27	DATA#28	DATA#29	DATA#30	DATA#31	DATA#32	DATA#33	DATA#34	DATA#35	DATA#36	DATA#37	DATA#38	DATA#39	DATA#40	DATA#41	DATA#42	DATA#43	DATA#44	DATA#45	DATA#46	DATA#47	DATA#48	DATA#49	DATA#50	DATA#51	DATA#52	DATA#53	DATA#54	DATA#55	DATA#56	DATA#57	DATA#58	DATA#59	DATA#60	DATA#61	DATA#62	DATA#63	DATA#64	DATA#65	DATA#66	DATA#67	DATA#68	DATA#69	DATA#70	DATA#71	DATA#72	DATA#73	DATA#74	DATA#75	DATA#76	DATA#77	DATA#78	DATA#79	DATA#80	DATA#81	DATA#82	DATA#83	DATA#84	DATA#85	DATA#86	DATA#87	DATA#88	DATA#89	DATA#90	DATA#91	DATA#92	DATA#93	DATA#94	DATA#95	DATA#96	DATA#97	DATA#98	DATA#99	DATA#100	DATA#101	DATA#102	DATA#103	DATA#104	DATA#105	DATA#106	DATA#107	DATA#108	DATA#109	DATA#110	DATA#111	DATA#112	DATA#113	DATA#114	DATA#115	DATA#116	DATA#117	DATA#118	DATA#119	DATA#120	DATA#121	DATA#122	DATA#123	DATA#124	DATA#125	DATA#126	DATA#127	DATA#128	DATA#129	DATA#130	DATA#131	DATA#132	DATA#133	DATA#134	DATA#135	DATA#136	DATA#137	DATA#138	DATA#139	DATA#140	DATA#141	DATA#142	DATA#143	DATA#144	DATA#145	DATA#146	DATA#147	DATA#148	DATA#149	DATA#150	DATA#151	DATA#152	DATA#153	DATA#154	DATA#155	DATA#156	DATA#157	DATA#158	DATA#159	DATA#160	DATA#161	DATA#162	DATA#163	DATA#164	DATA#165	DATA#166	DATA#167	DATA#168	DATA#169	DATA#170	DATA#171	DATA#172	DATA#173	DATA#174	DATA#175	DATA#176	DATA#177	DATA#178	DATA#179	DATA#180	DATA#181	DATA#182	DATA#183	DATA#184	DATA#185	DATA#186	DATA#187	DATA#188	DATA#189	DATA#190	DATA#191	DATA#192	DATA#193	DATA#194	DATA#195	DATA#196	DATA#197	DATA#198	DATA#199	DATA#200	DATA#201	DATA#202	DATA#203	DATA#204	DATA#205	DATA#206	DATA#207	DATA#208	DATA#209	DATA#210	DATA#211	DATA#212	DATA#213	DATA#214	DATA#215	DATA#216	DATA#217	DATA#218	DATA#219	DATA#220	DATA#221	DATA#222	DATA#223	DATA#224	DATA#225	DATA#226	DATA#227	DATA#228	DATA#229	DATA#230	DATA#231	DATA#232	DATA#233	DATA#234	DATA#235	DATA#236	DATA#237	DATA#238	DATA#239	DATA#240	DATA#241	DATA#242	DATA#243	DATA#244	DATA#245	DATA#246	DATA#247	DATA#248	DATA#249	DATA#250	DATA#251	DATA#252	DATA#253	DATA#254	DATA#255	DATA#256	DATA#257	DATA#258	DATA#259	DATA#260	DATA#261	DATA#262	DATA#263	DATA#264	DATA#265	DATA#266	DATA#267	DATA#268	DATA#269	DATA#270	DATA#271	DATA#272	DATA#273	DATA#274	DATA#275	DATA#276	DATA#277	DATA#278	DATA#279	DATA#280	DATA#281	DATA#282	DATA#283	DATA#284	DATA#285	DATA#286	DATA#287	DATA#288	DATA#289	DATA#290	DATA#291	DATA#292	DATA#293	DATA#294	DATA#295	DATA#296	DATA#297	DATA#298	DATA#299	DATA#300	DATA#301	DATA#302	DATA#303	DATA#304	DATA#305	DATA#306	DATA#307	DATA#308	DATA#309	DATA#310	DATA#311	DATA#312	DATA#313	DATA#314	DATA#315	DATA#316	DATA#317	DATA#318	DATA#319	DATA#320	DATA#321	DATA#322	DATA#323	DATA#324	DATA#325	DATA#326	DATA#327	DATA#328	DATA#329	DATA#330	DATA#331	DATA#332	DATA#333	DATA#334	DATA#335	DATA#336	DATA#337	DATA#338	DATA#339	DATA#340	DATA#341	DATA#342	DATA#343	DATA#344	DATA#345	DATA#346	DATA#347	DATA#348	DATA#349	DATA#350	DATA#351	DATA#352	DATA#353	DATA#354	DATA#355	DATA#356	DATA#357	DATA#358	DATA#359	DATA#360	DATA#361	DATA#362	DATA#363	DATA#364	DATA#365	DATA#366	DATA#367	DATA#368	DATA#369	DATA#370	DATA#371	DATA#372	DATA#373	DATA#374	DATA#375	DATA#376	DATA#377	DATA#378	DATA#379	DATA#380	DATA#381	DATA#382	DATA#383	DATA#384	DATA#385	DATA#386	DATA#387	DATA#388	DATA#389	DATA#390	DATA#391	DATA#392	DATA#393	DATA#394	DATA#395	DATA#396	DATA#397	DATA#398	DATA#399	DATA#400	DATA#401	DATA#402	DATA#403	DATA#404	DATA#405	DATA#406	DATA#407	DATA#408	DATA#409	DATA#410	DATA#411	DATA#412	DATA#413	DATA#414	DATA#415	DATA#416	DATA#417	DATA#418	DATA#419	DATA#420	DATA#421	DATA#422	DATA#423	DATA#424	DATA#425	DATA#426	DATA#427	DATA#428	DATA#429	DATA#430	DATA#431	DATA#432	DATA#433	DATA#434	DATA#435	DATA#436	DATA#437	DATA#438	DATA#439	DATA#440	DATA#441	DATA#442	DATA#443	DATA#444	DATA#445	DATA#446	DATA#447	DATA#448	DATA#449	DATA#450	DATA#451	DATA#452	DATA#453	DATA#454	DATA#455	DATA#456	DATA#457	DATA#458	DATA#459	DATA#460	DATA#461	DATA#462	DATA#463	DATA#464	DATA#465	DATA#466	DATA#467	DATA#468	DATA#469	DATA#470	DATA#471	DATA#472	DATA#473	DATA#474	DATA#475	DATA#476	DATA#477	DATA#478	DATA#479	DATA#480	DATA#481	DATA#482	DATA#483	DATA#484	DATA#485	DATA#486	DATA#487	DATA#488	DATA#489	DATA#490	DATA#491	DATA#492	DATA#493	DATA#494	DATA#495	DATA#496	DATA#497	DATA#498	DATA#499	DATA#500	DATA#501	DATA#502	DATA#503	DATA#504	DATA#505	DATA#506	DATA#507	DATA#508	DATA#509	DATA#510	DATA#511	DATA#512	DATA#513	DATA#514	DATA#515	DATA#516	DATA#517	DATA#518	DATA#519	DATA#520	DATA#521	DATA#522	DATA#523	DATA#524	DATA#525	DATA#526	DATA#527	DATA#528	DATA#529	DATA#530	DATA#531	DATA#532	DATA#533	DATA#534	DATA#535	DATA#536	DATA#537	DATA#538	DATA#539	DATA#540	DATA#541	DATA#542	DATA#543	DATA#544	DATA#545	DATA#546	DATA#547	DATA#548	DATA#549	DATA#550	DATA#551	DATA#552	DATA#553	DATA#554	DATA#555	DATA#556	DATA#557	DATA#558	DATA#559	DATA#560	DATA#561	DATA#562	DATA#563	DATA#564	DATA#565	DATA#566	DATA#567	DATA#568	DATA#569	DATA#570	DATA#571	DATA#572	DATA#573	DATA#574	DATA#575	DATA#576	DATA#577	DATA#578	DATA#579	DATA#580	DATA#581	DATA#582	DATA#583	DATA#584	DATA#585	DATA#586	DATA#587	DATA#588	DATA#589	DATA#590	DATA#591	DATA#592	DATA#593	DATA#594	DATA#595	DATA#596	DATA#597	DATA#598	DATA#599	DATA#600	DATA#601	DATA#602	DATA#603	DATA#604	DATA#605	DATA#606	DATA#607	DATA#608	DATA#609	DATA#610	DATA#611	DATA#612	DATA#613	DATA#614	DATA#615	DATA#616	DATA#617	DATA#618	DATA#619	DATA#620	DATA#621	DATA#622	DATA#623	DATA#624	DATA#625	DATA#626	DATA#627	DATA#628	DATA#629	DATA#630	DATA#631	DATA#632	DATA#633	DATA#634	DATA#635	DATA#636	DATA#637	DATA#638	DATA#639	DATA#640	DATA#641	DATA#642	DATA#643	DATA#644	DATA#645	DATA#646	DATA#647	DATA#648	DATA#649	DATA#650	DATA#651	DATA#652	DATA#653	DATA#654	DATA#655	DATA#656	DATA#657	DATA#658	DATA#659	DATA#660	DATA#661	DATA#662	DATA#663	DATA#664	DATA#665	DATA#666	DATA#667	DATA#668	DATA#669	DATA#670	DATA#671	DATA#672	DATA#673	DATA#674	DATA#675	DATA#676	DATA#677	DATA#678	DATA#679	DATA#680	DATA#681	DATA#682	DATA#683	DATA#684	DATA#685	DATA#686	DATA#687	DATA#688	DATA#689	DATA#690	DATA#691	DATA#692	DATA#693	DATA#694	DATA#695	DATA#696	DATA#697	DATA#698	DATA#699	DATA#700	DATA#701	DATA#702	DATA#703	DATA#704	DATA#705	DATA#706	DATA#707	DATA#708	DATA#709	DATA#710	DATA#711	DATA#712	DATA#713	DATA#714	DATA#715	DATA#716	DATA#717	DATA#718	DATA#719	DATA#720	DATA#721	DATA#722	DATA#723	DATA#724	DATA#725	DATA#726	DATA#727	DATA#728	DATA#729	DATA#730	DATA#731	DATA#732	DATA#733	DATA#734	DATA#735	DATA#736	DATA#737	DATA#738	DATA#739	DATA#740	DATA#741	DATA#742	DATA#743	DATA#744	DATA#745	DATA#746	DATA#747	DATA#748	DATA#749	DATA#750	DATA#751	DATA#752	DATA#753	DATA#754	DATA#755	DATA#756	DATA#757	DATA#758	DATA#759	DATA#760	DATA#761	DATA#762	DATA#763	DATA#764	DATA#765	DATA#766	DATA#767	DATA#768	DATA#769	DATA#770	DATA#771	DATA#772	DATA#773	DATA#774	DATA#775	DATA#776	DATA#777	DATA#778	DATA#779	DATA#780	DATA#781	DATA#782	DATA#783	DATA#784	DATA#785	DATA#786	DATA#787	DATA#788	DATA#789	DATA#790	DATA#791	DATA#792	DATA#793	DATA#794	DATA#795	DATA#796	DATA#797	DATA#798	DATA#799	DATA#800	DATA#801	DATA#802	DATA#803	DATA#804	DATA#805	DATA#806	DATA#807	DATA#808	DATA#809	DATA#810	DATA#811	DATA#812	DATA#813	DATA#814	DATA#815	DATA#816	DATA#817	DATA#818	DATA#819	DATA#820	DATA#821	DATA#822	DATA#823	DATA#824	DATA#825	DATA#826	DATA#827	DATA#828	DATA#829	DATA#830	DATA#831	DATA#832	DATA#833	DATA#834	DATA#835	DATA#836	DATA#837	DATA#838	DATA#839	DATA#840	DATA#841	DATA#842	DATA#843	DATA#844	DATA#845	DATA#846	DATA#847	DATA#848	DATA#849	DATA#850	DATA#851	DATA#852	DATA#853	DATA#854	DATA#855	DATA#856	DATA#857	DATA#858	DATA#859	DATA#860	DATA#861	DATA#862	DATA#863	DATA#864	DATA#865	DATA#866	DATA#867	DATA#868	DATA#869	DATA#870	DATA#871	DATA#872	DATA#873	DATA#874	DATA#875	DATA#876	DATA#877	DATA#878	DATA#879	DATA#880	DATA#881	DATA#882	DATA#883	DATA#884	DATA#885	DATA#886	DATA#887	DATA#888	DATA#889	DATA#890	DATA#891	DATA#892	DATA#893	DATA#894	DATA#895	DATA#896	DATA#897	DATA#898	DATA#899	DATA#900	DATA#901	DATA#902	DATA#903	DATA#904	DATA#905	DATA#906	DATA#907	DATA#908	DATA#909	DATA#910	DATA#911	DATA#912	DATA#913	DATA#914	DATA#915	DATA#916	DATA#917	DATA#918	DATA#919	DATA#920	DATA#921	DATA#922	DATA#923	DATA#924	DATA#925	DATA#926	DATA#927	DATA#928	DATA#929	DATA#930	DATA#931	DATA#932	DATA#933	DATA#934	DATA#935	DATA#936	DATA#937	DATA#938	DATA#939	DATA#940	DATA#941	DATA#942	DATA#943	DATA#944	DATA#945	DATA#946	DATA#947	DATA#948	DATA#949	DATA#950	DATA#951	DATA#952	DATA#953	DATA#954	DATA#955	DATA#956	DATA#957	DATA#958	DATA#959	DATA#960	DATA#961	DATA#962	DATA#963	DATA#964	DATA#965	DATA#966	DATA#967	DATA#968	DATA#969	DATA#970	DATA#971	DATA#972	DATA#973	DATA#974	DATA#975	DATA#976	DATA#977	DATA#978	DATA#979	DATA#980	DATA#981	DATA#982	DATA#983	DATA#984	DATA#985	DATA#986	DATA#987	DATA#988	DATA#989	DATA#990	DATA#991	DATA#992	DATA#993	DATA#994	DATA#995	DATA#996	DATA#997	DATA#998	DATA#999	DATA#1000
-----------	----------	--------	--------	--------	--------	--------	--------	--------	--------	--------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	----------	-----------

BLUNDER_1	L	5	65000.0	0.0	306.9	237.1	306.9	237.1	306.9	30.0	-3.0	NORM_ESC_1	R	6	67000.0	0.0	310.5	237.9	22.0	50.0	310.5	0	T	2.9	821.3	2260.9
BLUNDER_1	L	1	65000.0	0.0	254.9	173.8	254.9	173.8	254.9	30.0	-3.0	NORM_ESC_1	R	5	67000.0	0.0	308.3	237.0	22.0	42.0	308.3	0	T	4.3	735.6	1680.3
BLUNDER_1	L	1	65000.0	0.0	257.1	168.4	257.1	168.4	257.1	30.0	-3.0	NORM_ESC_1	R	5	67250.0	0.0	305.3	237.3	22.0	42.0	305.3	0	T	1.7	685.0	2227.6
BLUNDER_1	L	2	65000.0	0.0	246.8	183.7	246.8	183.7	246.8	30.0	-3.0	NORM_ESC_1	R	5	67250.0	0.0	303.4	237.0	22.0	42.0	303.4	0	T	-3.1	994.7	2405.8
BLUNDER_1	L	5	65000.0	0.0	307.2	236.9	307.2	236.9	307.2	30.0	-3.0	NORM_ESC_1	R	4	67250.0	0.0	306.9	237.0	22.0	33.0	306.9	0	T	6.5	1390.1	2001.9
BLUNDER_1	L	5	65000.0	0.0	305.2	238.2	305.2	238.2	305.2	30.0	-3.0	NORM_ESC_1	R	3	67250.0	0.0	256.8	193.2	22.0	25.0	256.8	0	T	6.8	3250.3	3510.0
BLUNDER_1	L	3	65000.0	0.0	254.6	179.8	254.6	179.8	254.6	30.0	-3.0	NORM_ESC_1	R	5	67500.0	0.0	301.8	234.4	22.0	42.0	301.8	0	T	-2.1	480.8	2707.9
BLUNDER_1	L	5	65000.0	0.0	306.8	240.7	306.8	240.7	306.8	30.0	-3.0	NORM_ESC_1	R	6	67500.0	0.0	305.8	235.8	22.0	50.0	305.8	0	T	2.5	1570.3	2724.9
BLUNDER_1	L	5	65000.0	0.0	306.5	236.1	306.5	236.1	306.5	30.0	-3.0	NORM_ESC_1	R	4	67500.0	0.0	304.1	235.5	22.0	42.0	304.1	0	T	5.6	1562.3	2265.2
BLUNDER_1	L	2	65000.0	0.0	249.4	187.5	249.4	187.5	249.4	30.0	-3.0	NORM_ESC_1	R	4	67500.0	0.0	301.3	236.7	22.0	33.0	301.3	0	T	-0.1	715.1	2338.2
BLUNDER_1	L	4	65000.0	0.0	302.2	236.0	302.2	236.0	302.2	30.0	-3.0	NORM_ESC_1	R	6	67500.0	0.0	301.1	239.7	22.0	50.0	301.1	0	T	4.3	1846.6	2715.7
BLUNDER_1	L	1	65000.0	0.0	284.5	165.1	284.5	165.1	284.5	30.0	-3.0	NORM_ESC_1	R	5	67750.0	0.0	301.0	238.7	22.0	42.0	301.0	0	T	9.6	309.4	1233.5
BLUNDER_1	L	2	65000.0	0.0	249.4	181.3	249.4	181.3	249.4	30.0	-3.0	NORM_ESC_1	R	5	67750.0	0.0	305.4	235.2	22.0	42.0	305.4	0	T	5.3	799.1	2111.6
BLUNDER_1	L	3	65000.0	0.0	251.4	184.1	251.4	184.1	251.4	30.0	-3.0	NORM_ESC_1	R	5	67750.0	0.0	302.9	231.0	22.0	42.0	302.9	0	T	8.7	544.1	1299.6
BLUNDER_1	L	4	65000.0	0.0	305.2	235.7	305.2	235.7	305.2	30.0	-3.0	NORM_ESC_1	R	1	68000.0	0.0	249.9	166.4	22.0	33.0	249.9	0	T	7.7	4227.0	4327.7
BLUNDER_1	L	2	65000.0	0.0	259.7	182.6	259.7	182.6	259.7	30.0	-3.0	NORM_ESC_1	R	5	68000.0	0.0	308.0	238.3	22.0	42.0	308.0	0	T	-8.7	64.2	2461.8
BLUNDER_1	L	5	65000.0	0.0	308.8	236.4	308.8	236.4	308.8	30.0	-3.0	NORM_ESC_1	R	5	68000.0	0.0	303.4	235.2	22.0	42.0	303.4	0	T	3.6	2184.1	3131.0
BLUNDER_1	L	3	65000.0	0.0	249.6	183.1	249.6	183.1	249.6	30.0	-3.0	NORM_ESC_1	R	5	68000.0	0.0	309.6	240.6	22.0	42.0	309.6	0	T	8.2	601.7	1571.1
BLUNDER_1	L	5	65000.0	0.0	303.3	234.6	303.3	234.6	303.3	30.0	-3.0	NORM_ESC_1	R	6	68250.0	0.0	309.6	235.6	22.0	50.0	309.6	0	T	3.8	2172.6	3298.7
BLUNDER_1	L	6	65000.0	0.0	303.7	243.6	303.7	243.6	303.7	30.0	-3.0	NORM_ESC_1	R	5	68250.0	0.0	298.6	238.9	22.0	42.0	298.6	0	T	3.4	2453.1	3504.0
BLUNDER_1	L	5	65000.0	0.0	308.4	236.6	308.4	236.6	308.4	30.0	-3.0	NORM_ESC_1	R	5	68250.0	0.0	306.5	236.5	22.0	42.0	306.5	0	T	8.1	2422.4	2922.1
BLUNDER_1	L	1	65000.0	0.0	251.7	168.2	251.7	168.2	251.7	30.0	-3.0	NORM_ESC_1	R	5	68250.0	0.0	302.5	232.4	22.0	42.0	302.5	0	T	12.0	134.6	876.9
BLUNDER_1	L	4	65000.0	0.0	299.1	239.5	299.1	239.5	299.1	30.0	-3.0	NORM_ESC_1	R	2	68500.0	0.0	258.8	185.3	22.0	17.0	258.8	0	T	6.7	4196.5	4500.0
BLUNDER_1	L	5	65000.0	0.0	302.8	238.3	302.8	238.3	302.8	30.0	-3.0	NORM_ESC_1	R	2	68500.0	0.0	259.4	185.7	22.0	17.0	259.4	0	T	4.2	4332.6	4551.5
BLUNDER_1	L	5	65000.0	0.0	303.1	237.6	303.1	237.6	303.1	30.0	-3.0	NORM_ESC_1	R	4	68500.0	0.0	306.2	239.0	22.0	33.0	306.2	0	T	7.3	2405.3	3000.3
BLUNDER_1	L	5	65000.0	0.0	303.7	233.6	303.7	233.6	303.7	30.0	-3.0	NORM_ESC_1	R	5	68500.0	0.0	299.7	230.9	22.0	42.0	299.7	0	T	6.5	2694.4	3094.7

TABLE B2.-AC_1.track Output File

*ESA

run1

*FLOAT

T1	RWY	1isL	X1	Y1	Z1	LEG1	HEAD1	V1	BANK1	SLOPE1
0.5	1		-64848.0	-1963.7	3398.5	1	0.2	304.0	0.0	-3.0
1.0	1		-64696.0	-1963.1	3390.5	1	0.2	304.0	0.0	-3.0
1.5	1		-64544.0	-1962.5	3382.6	1	0.2	304.0	0.0	-3.0
2.0	1		-64392.0	-1961.8	3374.6	1	0.2	304.0	0.0	-3.0
2.5	1		-64240.0	-1961.2	3366.7	1	0.2	304.0	0.0	-3.0
3.0	1		-64088.0	-1960.6	3358.7	1	0.2	304.0	0.0	-3.0
3.5	1		-63936.0	-1960.0	3350.8	1	0.2	304.0	0.0	-3.0
4.0	1		-63784.0	-1959.4	3342.8	1	0.2	304.0	0.0	-3.0
4.5	1		-63632.0	-1958.7	3334.9	1	0.2	304.0	0.0	-3.0
5.0	1		-63480.0	-1958.1	3326.9	1	0.2	304.0	0.0	-3.0
5.5	1		-63328.0	-1957.5	3318.9	1	0.2	304.0	0.0	-3.0
6.0	1		-63176.0	-1956.9	3311.0	1	0.2	304.0	0.0	-3.0
6.5	1		-63023.9	-1956.3	3303.0	1	0.2	304.0	0.0	-3.0
7.0	1		-62871.9	-1955.7	3295.1	1	0.2	304.0	0.0	-3.0
7.5	1		-62719.9	-1955.0	3287.1	1	0.2	304.0	0.0	-3.0
8.0	1		-62567.9	-1954.4	3279.2	1	0.2	304.0	0.0	-3.0
8.5	1		-62415.9	-1953.8	3271.2	1	0.2	304.0	0.0	-3.0
9.0	1		-62263.9	-1953.2	3263.3	1	0.2	304.0	0.0	-3.0
9.5	1		-62111.9	-1952.6	3255.3	1	0.2	304.0	0.0	-3.0
10.0	1		-61959.9	-1951.9	3247.3	1	0.2	304.0	0.0	-3.0
10.5	1		-61807.9	-1951.3	3239.4	1	0.2	304.0	0.0	-3.0
11.0	1		-61655.9	-1950.7	3231.4	1	0.2	304.0	0.0	-3.0
11.5	1		-61503.9	-1948.4	3223.5	1	1.6	304.0	26.4	-3.0
12.0	1		-61352.1	-1942.1	3215.5	1	3.1	304.0	26.4	-3.0
12.5	1		-61200.4	-1931.8	3207.6	1	4.6	304.0	26.4	-3.0
13.0	1		-61049.1	-1917.6	3199.6	1	6.1	304.0	26.4	-3.0
13.5	1		-60898.2	-1899.4	3191.7	1	7.6	304.0	26.4	-3.0
14.0	1		-60747.8	-1877.3	3183.7	1	9.1	304.0	26.4	-3.0
14.5	1		-60598.1	-1851.2	3175.8	1	10.6	304.0	26.4	-3.0
15.0	1		-60449.1	-1821.2	3167.8	1	12.1	304.0	26.4	-3.0
15.5	1		-60300.9	-1787.4	3159.8	1	13.6	304.0	26.4	-3.0
16.0	1		-60153.7	-1749.7	3151.9	1	15.1	304.0	26.4	-3.0
16.5	1		-60007.5	-1708.1	3143.9	1	16.6	304.0	26.4	-3.0
17.0	1		-59862.4	-1662.7	3136.0	1	18.1	304.0	26.4	-3.0
17.5	1		-59718.6	-1613.5	3128.0	1	19.6	304.0	26.4	-3.0
18.0	1		-59576.1	-1560.6	3120.1	1	21.1	304.0	26.4	-3.0
18.5	1		-59435.1	-1504.0	3112.1	1	22.6	304.0	26.4	-3.0
19.0	1		-59295.6	-1443.7	3104.2	1	24.1	304.0	26.4	-3.0
19.5	1		-59157.7	-1379.8	3096.2	1	25.6	304.0	26.4	-3.0
20.0	1		-59021.5	-1312.3	3088.2	1	27.1	304.0	26.4	-3.0
20.5	1		-58887.1	-1241.2	3080.3	1	28.6	304.0	26.4	-3.0
21.0	1		-58754.7	-1166.7	3072.3	2	30.0	304.0	0.0	-3.0
21.5	1		-58623.0	-1090.7	3064.4	2	30.0	304.0	0.0	-3.0
22.0	1		-58491.4	-1014.7	3056.4	2	30.0	304.0	0.0	-3.0
22.5	1		-58359.8	-938.7	3048.5	2	30.0	304.0	0.0	-3.0
23.0	1		-58228.1	-862.7	3040.5	2	30.0	304.0	0.0	-3.0
23.5	1		-58096.5	-786.7	3032.6	2	30.0	304.0	0.0	-3.0
24.0	1		-57964.8	-710.7	3024.6	2	30.0	304.0	0.0	-3.0
24.5	1		-57833.2	-634.7	3016.6	2	30.0	304.0	0.0	-3.0
25.0	1		-57701.6	-558.7	3008.7	2	30.0	304.0	0.0	-3.0
25.5	1		-57569.9	-482.7	3000.7	2	30.0	304.0	0.0	-3.0
26.0	1		-57438.3	-406.7	2992.8	2	30.0	304.0	0.0	-3.0
26.5	1		-57306.6	-330.7	2984.8	2	30.0	304.0	0.0	-3.0
27.0	1		-57175.0	-254.7	2976.9	2	30.0	304.0	0.0	-3.0
27.5	1		-57043.3	-178.7	2968.9	2	30.0	304.0	0.0	-3.0
28.0	1		-56911.7	-102.7	2961.0	2	30.0	304.0	0.0	-3.0
28.5	1		-56780.1	-26.7	2953.0	2	30.0	304.0	0.0	-3.0
29.0	1		-56648.4	49.3	2945.1	2	30.0	304.0	0.0	-3.0
29.5	1		-56516.8	125.3	2937.1	2	30.0	304.0	0.0	-3.0
30.0	1		-56385.1	201.3	2929.1	2	30.0	304.0	0.0	-3.0
30.5	1		-56253.5	277.3	2921.2	2	30.0	304.0	0.0	-3.0
31.0	1		-56121.9	353.3	2913.2	2	30.0	304.0	0.0	-3.0
31.5	1		-55990.2	429.3	2905.3	2	30.0	304.0	0.0	-3.0
32.0	1		-55858.6	505.3	2897.3	2	30.0	304.0	0.0	-3.0
32.5	1		-55726.9	581.3	2889.4	2	30.0	304.0	0.0	-3.0
33.0	1		-55595.3	657.3	2881.4	2	30.0	304.0	0.0	-3.0
33.5	1		-55463.7	733.3	2873.5	2	30.0	304.0	0.0	-3.0
34.0	1		-55332.0	809.3	2865.5	2	30.0	304.0	0.0	-3.0

34.5	1	-55200.4	885.3	2857.5	2	30.0	304.0	0.0	-3.0
35.0	1	-55068.7	961.3	2849.6	2	30.0	304.0	0.0	-3.0
35.5	1	-54937.1	1037.3	2841.6	2	30.0	304.0	0.0	-3.0
36.0	1	-54805.5	1113.3	2833.7	2	30.0	304.0	0.0	-3.0
36.5	1	-54673.8	1189.3	2825.7	2	30.0	304.0	0.0	-3.0
37.0	1	-54542.2	1265.3	2817.8	2	30.0	304.0	0.0	-3.0
37.5	1	-54410.5	1341.3	2809.8	2	30.0	304.0	0.0	-3.0
38.0	1	-54278.9	1417.3	2801.9	2	30.0	304.0	0.0	-3.0
38.5	1	-54147.3	1493.3	2793.9	2	30.0	304.0	0.0	-3.0
39.0	1	-54015.6	1569.3	2786.0	2	30.0	304.0	0.0	-3.0
39.5	1	-53884.0	1645.3	2778.0	2	30.0	304.0	0.0	-3.0
40.0	1	-53752.3	1721.3	2770.0	2	30.0	304.0	0.0	-3.0
40.5	1	-53620.7	1797.3	2762.1	2	30.0	304.0	0.0	-3.0
41.0	1	-53489.1	1873.3	2754.1	2	30.0	304.0	0.0	-3.0
41.5	1	-53357.4	1949.3	2746.2	2	30.0	304.0	0.0	-3.0
42.0	1	-53225.8	2025.3	2738.2	2	30.0	304.0	0.0	-3.0
42.5	1	-53094.1	2101.3	2730.3	2	30.0	304.0	0.0	-3.0
43.0	1	-52962.5	2177.4	2722.3	2	30.0	304.0	0.0	-3.0
43.5	1	-52830.8	2253.4	2714.4	2	30.0	304.0	0.0	-3.0
44.0	1	-52699.2	2329.4	2706.4	2	30.0	304.0	0.0	-3.0
44.5	1	-52567.6	2405.4	2698.4	2	30.0	304.0	0.0	-3.0
45.0	1	-52435.9	2481.4	2690.5	2	30.0	304.0	0.0	-3.0
45.5	1	-52304.3	2557.4	2682.5	2	30.0	304.0	0.0	-3.0
46.0	1	-52172.6	2633.4	2674.6	2	30.0	304.0	0.0	-3.0
46.5	1	-52041.0	2709.4	2666.6	2	30.0	304.0	0.0	-3.0
47.0	1	-51909.4	2785.4	2658.7	2	30.0	304.0	0.0	-3.0
47.5	1	-51777.7	2861.4	2650.7	2	30.0	304.0	0.0	-3.0
48.0	1	-51646.1	2937.4	2642.8	2	30.0	304.0	0.0	-3.0
48.5	1	-51514.4	3013.4	2634.8	2	30.0	304.0	0.0	-3.0
49.0	1	-51382.8	3089.4	2626.9	2	30.0	304.0	0.0	-3.0
49.5	1	-51251.2	3165.4	2618.9	2	30.0	304.0	0.0	-3.0
50.0	1	-51119.5	3241.4	2610.9	2	30.0	304.0	0.0	-3.0
50.5	1	-50987.9	3317.4	2603.0	2	30.0	304.0	0.0	-3.0
51.0	1	-50856.2	3393.4	2595.0	2	30.0	304.0	0.0	-3.0
51.5	1	-50724.6	3469.4	2587.1	2	30.0	304.0	0.0	-3.0
52.0	1	-50593.0	3545.4	2579.1	2	30.0	304.0	0.0	-3.0
52.5	1	-50461.3	3621.4	2571.2	2	30.0	304.0	0.0	-3.0
53.0	1	-50329.7	3697.4	2563.2	2	30.0	304.0	0.0	-3.0
53.5	1	-50198.0	3773.4	2555.3	2	30.0	304.0	0.0	-3.0
54.0	1	-50066.4	3849.4	2547.3	2	30.0	304.0	0.0	-3.0
54.5	1	-49934.8	3925.4	2539.3	2	30.0	304.0	0.0	-3.0
55.0	1	-49803.1	4001.4	2531.4	2	30.0	304.0	0.0	-3.0
55.5	1	-49671.5	4077.4	2523.4	2	30.0	304.0	0.0	-3.0
56.0	1	-49539.8	4153.4	2515.5	2	30.0	304.0	0.0	-3.0
56.5	1	-49408.2	4229.4	2507.5	2	30.0	304.0	0.0	-3.0
57.0	1	-49276.6	4305.4	2499.6	2	30.0	304.0	0.0	-3.0
57.5	1	-49144.9	4381.4	2491.6	2	30.0	304.0	0.0	-3.0
58.0	1	-49013.3	4457.4	2483.7	2	30.0	304.0	0.0	-3.0
58.5	1	-48881.6	4533.4	2475.7	2	30.0	304.0	0.0	-3.0
59.0	1	-48750.0	4609.4	2467.7	2	30.0	304.0	0.0	-3.0
59.5	1	-48618.3	4685.4	2459.8	2	30.0	304.0	0.0	-3.0
60.0	1	-48486.7	4761.4	2451.8	2	30.0	304.0	0.0	-3.0
60.5	1	-48355.1	4837.4	2443.9	2	30.0	304.0	0.0	-3.0
61.0	1	-48223.4	4913.4	2435.9	2	30.0	304.0	0.0	-3.0
61.5	1	-48091.8	4989.4	2428.0	2	30.0	304.0	0.0	-3.0
62.0	1	-47960.1	5065.4	2420.0	2	30.0	304.0	0.0	-3.0
62.5	1	-47828.5	5141.4	2412.1	2	30.0	304.0	0.0	-3.0
63.0	1	-47696.9	5217.4	2404.1	2	30.0	304.0	0.0	-3.0
63.5	1	-47565.2	5293.4	2396.2	2	30.0	304.0	0.0	-3.0
64.0	1	-47433.6	5369.4	2388.2	2	30.0	304.0	0.0	-3.0
64.5	1	-47301.9	5445.4	2380.2	2	30.0	304.0	0.0	-3.0
65.0	1	-47170.3	5521.4	2372.3	2	30.0	304.0	0.0	-3.0
65.5	1	-47038.7	5597.4	2364.3	2	30.0	304.0	0.0	-3.0
66.0	1	-46907.0	5673.4	2356.4	2	30.0	304.0	0.0	-3.0
66.5	1	-46775.4	5749.4	2348.4	2	30.0	304.0	0.0	-3.0
67.0	1	-46643.7	5825.4	2340.5	2	30.0	304.0	0.0	-3.0
67.5	1	-46512.1	5901.4	2332.5	2	30.0	304.0	0.0	-3.0
68.0	1	-46380.5	5977.4	2324.6	2	30.0	304.0	0.0	-3.0
68.5	1	-46248.8	6053.4	2316.6	2	30.0	304.0	0.0	-3.0
69.0	1	-46117.2	6129.4	2308.6	2	30.0	304.0	0.0	-3.0
69.5	1	-45985.5	6205.4	2300.7	2	30.0	304.0	0.0	-3.0
70.0	1	-45853.9	6281.4	2292.7	2	30.0	304.0	0.0	-3.0

70.5	1	-45722.3	6357.4	2284.8	2	30.0	304.0	0.0	-3.0
71.0	1	-45590.6	6433.4	2276.8	2	30.0	304.0	0.0	-3.0
71.5	1	-45459.0	6509.4	2268.9	2	30.0	304.0	0.0	-3.0
72.0	1	-45327.3	6585.4	2260.9	2	30.0	304.0	0.0	-3.0
72.5	1	-45195.7	6661.4	2253.0	2	30.0	304.0	0.0	-3.0
73.0	1	-45064.1	6737.4	2245.0	2	30.0	304.0	0.0	-3.0
73.5	1	-44932.4	6813.4	2237.1	2	30.0	304.0	0.0	-3.0
74.0	1	-44800.8	6889.4	2229.1	2	30.0	304.0	0.0	-3.0
74.5	1	-44669.1	6965.4	2221.1	2	30.0	304.0	0.0	-3.0
75.0	1	-44537.5	7041.4	2213.2	2	30.0	304.0	0.0	-3.0
75.5	1	-44405.8	7117.4	2205.2	2	30.0	304.0	0.0	-3.0
76.0	1	-44274.2	7193.4	2197.3	2	30.0	304.0	0.0	-3.0
76.5	1	-44142.6	7269.4	2189.3	2	30.0	304.0	0.0	-3.0

*ESA

run1

*FLOAT

T1	RWY	lisL	X1	Y1	Z1	LEG1	HEAD1	V1	BANK1	SLOPE1
0.5	1		-64850.1	-1929.3	3398.6	1	0.2	299.9	0.0	-3.0
1.0	1		-64700.1	-1928.8	3390.8	1	0.2	299.9	0.0	-3.0
1.5	1		-64550.2	-1928.2	3382.9	1	0.2	299.9	0.0	-3.0
2.0	1		-64400.3	-1927.7	3375.1	1	0.2	299.9	0.0	-3.0
2.5	1		-64250.3	-1927.2	3367.2	1	0.2	299.9	0.0	-3.0
3.0	1		-64100.4	-1926.6	3359.4	1	0.2	299.9	0.0	-3.0
3.5	1		-63950.4	-1926.1	3351.5	1	0.2	299.9	0.0	-3.0
4.0	1		-63800.5	-1925.6	3343.7	1	0.2	299.9	0.0	-3.0
4.5	1		-63650.6	-1925.0	3335.8	1	0.2	299.9	0.0	-3.0
5.0	1		-63500.6	-1924.5	3328.0	1	0.2	299.9	0.0	-3.0

TABLE B3.-AC_2.track Output File

*ESA

run1

*FLOAT

T2	RWY	2isR	X2	Y2	Z2	LEG2	HEAD2	V2	BANK2	SLOPE2
0.5	2		-62374.2	1830.8	3268.8	1	-0.1	251.6	0.0	-3.0
1.0	2		-62248.4	1830.6	3262.3	1	-0.1	251.6	0.0	-3.0
1.5	2		-62122.7	1830.3	3255.7	1	-0.1	251.6	0.0	-3.0
2.0	2		-61996.9	1830.0	3249.1	1	-0.1	251.6	0.0	-3.0
2.5	2		-61871.1	1829.8	3242.5	1	-0.1	251.6	0.0	-3.0
3.0	2		-61745.3	1829.5	3235.9	1	-0.1	251.6	0.0	-3.0
3.5	2		-61619.5	1829.2	3229.4	1	-0.1	251.6	0.0	-3.0
4.0	2		-61493.8	1829.0	3222.8	1	-0.1	251.6	0.0	-3.0
4.5	2		-61368.0	1828.7	3216.2	1	-0.1	251.6	0.0	-3.0
5.0	2		-61242.2	1828.5	3209.6	1	-0.1	251.6	0.0	-3.0
5.5	2		-61116.4	1828.2	3203.0	1	-0.1	251.6	0.0	-3.0
6.0	2		-60990.6	1827.9	3196.4	1	-0.1	251.6	0.0	-3.0
6.5	2		-60864.8	1827.7	3189.9	1	-0.1	251.6	0.0	-3.0
7.0	2		-60739.1	1827.4	3183.3	1	-0.1	251.6	0.0	-3.0
7.5	2		-60613.3	1827.1	3176.7	1	-0.1	251.6	0.0	-3.0
8.0	2		-60487.5	1826.9	3170.1	1	-0.1	251.6	0.0	-3.0
8.5	2		-60361.7	1826.6	3163.5	1	-0.1	251.6	0.0	-3.0
9.0	2		-60235.9	1826.3	3156.9	1	-0.1	251.6	0.0	-3.0
9.5	2		-60110.2	1826.1	3150.4	1	-0.1	251.6	0.0	-3.0
10.0	2		-59984.4	1825.8	3143.8	1	-0.1	251.6	0.0	-3.0
10.5	2		-59858.6	1825.6	3137.2	1	-0.1	251.6	0.0	-3.0
11.0	2		-59732.8	1825.3	3130.6	1	-0.1	251.6	0.0	-3.0
11.5	2		-59607.0	1825.0	3124.0	1	-0.1	251.6	0.0	-3.0
12.0	2		-59481.3	1824.8	3117.4	1	-0.1	251.6	0.0	-3.0
12.5	2		-59355.5	1824.5	3110.9	1	-0.1	251.6	0.0	-3.0
13.0	2		-59229.7	1824.2	3104.3	1	-0.1	251.6	0.0	-3.0
13.5	2		-59103.9	1824.0	3097.7	1	-0.1	251.6	0.0	-3.0
14.0	2		-58978.1	1823.7	3091.1	1	-0.1	251.6	0.0	-3.0
14.5	2		-58852.3	1823.4	3084.5	1	-0.1	251.6	0.0	-3.0
15.0	2		-58726.6	1823.2	3077.9	1	-0.1	251.6	0.0	-3.0
15.5	2		-58600.8	1822.9	3071.4	1	-0.1	251.6	0.0	-3.0
16.0	2		-58475.0	1822.6	3064.8	1	-0.1	251.6	0.0	-3.0
16.5	2		-58349.2	1822.4	3058.2	1	-0.1	251.6	0.0	-3.0
17.0	2		-58223.4	1822.1	3051.6	1	-0.1	251.6	0.0	-3.0
17.5	2		-58097.7	1821.9	3045.0	1	-0.1	251.6	0.0	-3.0
18.0	2		-57971.9	1821.6	3038.5	1	-0.1	251.6	0.0	-3.0
18.5	2		-57846.1	1821.3	3031.9	1	-0.1	251.6	0.0	-3.0
19.0	2		-57720.3	1821.1	3025.3	1	-0.1	251.6	0.0	-3.0
19.5	2		-57594.5	1820.8	3018.7	1	-0.1	251.6	0.0	-3.0
20.0	2		-57468.8	1820.5	3012.1	1	-0.1	251.6	0.0	-3.0
20.5	2		-57343.0	1820.3	3005.5	1	-0.1	251.6	0.0	-3.0
21.0	2		-57217.2	1820.0	2999.0	1	-0.1	251.6	0.0	-3.0
21.5	2		-57091.4	1819.7	2992.4	1	-0.1	251.6	0.0	-3.0
22.0	2		-56965.6	1819.5	2985.8	1	-0.1	251.6	0.0	-3.0
22.5	2		-56839.8	1819.2	2979.2	1	-0.1	251.6	0.0	-3.0
23.0	2		-56714.1	1819.0	2972.6	1	-0.1	251.6	0.0	-3.0
23.5	2		-56588.3	1818.7	2966.0	1	-0.1	251.6	0.0	-3.0
24.0	2		-56462.5	1818.4	2959.5	1	-0.1	251.6	0.0	-3.0
24.5	2		-56336.7	1818.2	2952.9	1	-0.1	251.6	0.0	-3.0
25.0	2		-56210.9	1817.9	2946.3	1	-0.1	251.6	0.0	-3.0
25.5	2		-56085.2	1817.6	2939.7	1	-0.1	251.6	0.0	-3.0
26.0	2		-55959.4	1817.4	2933.1	1	-0.1	251.6	0.0	-3.0
26.5	2		-55833.6	1817.1	2926.5	1	-0.1	251.6	0.0	-3.0
27.0	2		-55707.8	1818.5	2920.0	1	1.4	251.6	22.0	-3.0
27.5	2		-55582.1	1823.1	2913.4	1	2.8	251.6	22.0	-3.0
28.0	2		-55456.6	1830.9	2906.8	1	4.3	251.6	22.0	-3.0
28.5	2		-55331.3	1842.0	2900.2	1	5.8	251.6	22.0	-3.0
29.0	2		-55206.4	1856.3	2893.6	1	7.3	251.6	22.0	-3.0
29.5	2		-55081.8	1873.8	2887.0	1	8.7	251.6	22.0	-3.0
30.0	2		-54957.8	1894.5	2880.5	1	10.2	251.6	22.0	-3.0
30.5	2		-54834.3	1918.4	2873.9	1	11.7	251.6	22.0	-3.0
31.0	2		-54711.5	1945.5	2867.3	1	13.2	251.6	22.0	-3.0
31.5	2		-54589.4	1975.7	2860.7	1	14.6	251.6	22.0	-3.0
32.0	2		-54468.1	2009.1	2854.1	1	16.1	251.6	22.0	-3.0
32.5	2		-54347.8	2045.6	2847.6	1	17.6	251.6	22.0	-3.0
33.0	2		-54228.4	2085.1	2841.0	1	19.1	251.6	22.0	-3.0
33.5	2		-54110.1	2127.8	2834.4	1	20.6	251.6	22.0	-3.0
34.0	2		-53992.9	2173.5	2827.8	1	22.0	251.6	22.0	-3.0

34.5	2	-53876.9	2222.1	2821.2	1	23.5	251.6	22.0	-3.0
35.0	2	-53762.2	2273.8	2814.6	1	25.0	251.6	22.0	-3.0
35.5	2	-53648.9	2328.4	2808.1	1	26.5	251.6	22.0	-3.0
36.0	2	-53537.1	2385.9	2801.5	1	27.9	251.6	22.0	-3.0
36.5	2	-53426.7	2446.2	2794.9	1	29.4	251.6	22.0	-3.0
37.0	2	-53318.0	2509.4	2788.3	1	30.9	251.6	22.0	-3.0
37.5	2	-53210.9	2575.4	2781.7	1	32.4	251.6	22.0	-3.0
38.0	2	-53105.5	2644.1	2775.1	1	33.8	251.6	22.0	-3.0
38.5	2	-53002.0	2715.5	2768.6	1	35.3	251.6	22.0	-3.0
39.0	2	-52900.3	2789.5	2762.0	1	36.8	251.6	22.0	-3.0
39.5	2	-52800.6	2866.1	2755.4	1	38.3	251.6	22.0	-3.0
40.0	2	-52702.9	2945.3	2748.8	1	39.8	251.6	22.0	-3.0
40.5	2	-52607.2	3027.0	2742.2	1	41.2	251.6	22.0	-3.0
41.0	2	-52513.7	3111.1	2735.6	1	42.7	251.6	22.0	-3.0
41.5	2	-52422.4	3197.6	2729.1	1	44.2	251.6	22.0	-3.0
42.0	2	-52333.4	3286.4	2722.5	1	45.7	251.6	22.0	-3.0
42.5	2	-52246.6	3377.5	2715.9	1	47.1	251.6	22.0	-3.0
43.0	2	-52162.3	3470.8	2709.3	1	48.6	251.6	22.0	-3.0
43.5	2	-52080.4	3566.2	2702.7	1	50.1	251.6	22.0	-3.0
44.0	2	-52000.9	3663.7	2696.1	1	51.6	251.6	22.0	-3.0
44.5	2	-51924.0	3763.3	2689.6	1	53.0	251.6	22.0	-3.0
45.0	2	-51849.7	3864.7	2683.0	1	54.5	251.6	22.0	-3.0
45.5	2	-51777.4	3967.7	2689.3	2	55.0	251.6	0.0	5.7
46.0	2	-51705.3	4070.7	2701.8	2	55.0	251.6	0.0	5.7
46.5	2	-51633.1	4173.7	2714.3	2	55.0	251.6	0.0	5.7
47.0	2	-51561.0	4276.8	2726.8	2	55.0	251.6	0.0	5.7
47.5	2	-51488.8	4379.8	2739.3	2	55.0	251.6	0.0	5.7
48.0	2	-51416.7	4482.8	2751.8	2	55.0	251.6	0.0	5.7
48.5	2	-51344.5	4585.9	2764.3	2	55.0	251.6	0.0	5.7
49.0	2	-51272.4	4688.9	2776.8	2	55.0	251.6	0.0	5.7
49.5	2	-51200.2	4791.9	2789.3	2	55.0	251.6	0.0	5.7
50.0	2	-51128.1	4895.0	2801.8	2	55.0	251.6	0.0	5.7
50.5	2	-51055.9	4998.0	2814.3	2	55.0	251.6	0.0	5.7
51.0	2	-50983.8	5101.0	2826.8	2	55.0	251.6	0.0	5.7
51.5	2	-50911.7	5204.1	2839.3	2	55.0	251.6	0.0	5.7
52.0	2	-50839.5	5307.1	2851.8	2	55.0	251.6	0.0	5.7
52.5	2	-50767.4	5410.1	2864.3	2	55.0	251.6	0.0	5.7
53.0	2	-50695.2	5513.2	2876.8	2	55.0	251.6	0.0	5.7
53.5	2	-50623.1	5616.2	2889.3	2	55.0	251.6	0.0	5.7
54.0	2	-50550.9	5719.2	2901.8	2	55.0	251.6	0.0	5.7
54.5	2	-50478.8	5822.3	2914.3	2	55.0	251.6	0.0	5.7
55.0	2	-50406.6	5925.3	2926.8	2	55.0	251.6	0.0	5.7
55.5	2	-50334.5	6028.3	2939.3	2	55.0	251.6	0.0	5.7
56.0	2	-50262.3	6131.4	2951.8	2	55.0	251.6	0.0	5.7
56.5	2	-50190.2	6234.4	2964.3	2	55.0	251.6	0.0	5.7
57.0	2	-50118.0	6337.4	2976.8	2	55.0	251.6	0.0	5.7
57.5	2	-50045.9	6440.5	2989.3	2	55.0	251.6	0.0	5.7
58.0	2	-49973.7	6543.5	3001.8	2	55.0	251.6	0.0	5.7
58.5	2	-49901.6	6646.5	3014.3	2	55.0	251.6	0.0	5.7
59.0	2	-49829.4	6749.6	3026.8	2	55.0	251.6	0.0	5.7
59.5	2	-49757.3	6852.6	3039.3	2	55.0	251.6	0.0	5.7
60.0	2	-49685.1	6955.6	3051.8	2	55.0	251.6	0.0	5.7
60.5	2	-49613.0	7058.7	3064.3	2	55.0	251.6	0.0	5.7
61.0	2	-49540.8	7161.7	3076.8	2	55.0	251.6	0.0	5.7
61.5	2	-49468.7	7264.7	3089.3	2	55.0	251.6	0.0	5.7
62.0	2	-49396.5	7367.8	3101.8	2	55.0	251.6	0.0	5.7
62.5	2	-49324.4	7470.8	3114.3	2	55.0	251.6	0.0	5.7
63.0	2	-49252.2	7573.8	3126.8	2	55.0	251.6	0.0	5.7
63.5	2	-49180.1	7676.9	3139.3	2	55.0	251.6	0.0	5.7
64.0	2	-49107.9	7779.9	3151.8	2	55.0	251.6	0.0	5.7
64.5	2	-49035.8	7882.9	3164.3	2	55.0	251.6	0.0	5.7
65.0	2	-48963.6	7986.0	3176.8	2	55.0	251.6	0.0	5.7
65.5	2	-48891.5	8089.0	3189.3	2	55.0	251.6	0.0	5.7
66.0	2	-48819.3	8192.0	3201.8	2	55.0	251.6	0.0	5.7
66.5	2	-48747.2	8295.1	3214.3	2	55.0	251.6	0.0	5.7
67.0	2	-48675.1	8398.1	3226.8	2	55.0	251.6	0.0	5.7
67.5	2	-48602.9	8501.1	3239.3	2	55.0	251.6	0.0	5.7
68.0	2	-48530.8	8604.2	3251.8	2	55.0	251.6	0.0	5.7
68.5	2	-48458.6	8707.2	3264.3	2	55.0	251.6	0.0	5.7
69.0	2	-48386.5	8810.2	3276.8	2	55.0	251.6	0.0	5.7
69.5	2	-48314.3	8913.3	3289.3	2	55.0	251.6	0.0	5.7
70.0	2	-48242.2	9016.3	3301.8	2	55.0	251.6	0.0	5.7

70.5	2	-48170.0	9119.3	3314.3	2	55.0	251.6	0.0	5.7
71.0	2	-48097.9	9222.4	3326.8	2	55.0	251.6	0.0	5.7
71.5	2	-48025.7	9325.4	3339.3	2	55.0	251.6	0.0	5.7
72.0	2	-47953.6	9428.4	3351.8	2	55.0	251.6	0.0	5.7
72.5	2	-47881.4	9531.5	3364.3	2	55.0	251.6	0.0	5.7
73.0	2	-47809.3	9634.5	3376.8	2	55.0	251.6	0.0	5.7
73.5	2	-47737.1	9737.5	3389.3	2	55.0	251.6	0.0	5.7
74.0	2	-47665.0	9840.6	3401.8	2	55.0	251.6	0.0	5.7
74.5	2	-47592.8	9943.6	3414.3	2	55.0	251.6	0.0	5.7
75.0	2	-47520.7	10046.6	3426.8	2	55.0	251.6	0.0	5.7
75.5	2	-47448.5	10149.7	3439.3	2	55.0	251.6	0.0	5.7
76.0	2	-47376.4	10252.7	3451.8	2	55.0	251.6	0.0	5.7
76.5	2	-47304.2	10355.7	3464.3	2	55.0	251.6	0.0	5.7

*ESA

run1

*FLOAT

T2	RWY	2isR	X2	Y2	Z2	LEG2	HEAD2	V2	BANK2	SLOPE2
0.5	2		-62345.6	1616.0	3267.4	1	0.1	308.8	0.0	-3.0
1.0	2		-62191.2	1616.2	3259.3	1	0.1	308.8	0.0	-3.0
1.5	2		-62036.8	1616.4	3251.2	1	0.1	308.8	0.0	-3.0
2.0	2		-61882.4	1616.7	3243.1	1	0.1	308.8	0.0	-3.0
2.5	2		-61728.0	1616.9	3235.0	1	0.1	308.8	0.0	-3.0
3.0	2		-61573.6	1617.1	3226.9	1	0.1	308.8	0.0	-3.0
3.5	2		-61419.2	1617.3	3218.9	1	0.1	308.8	0.0	-3.0
4.0	2		-61264.8	1617.5	3210.8	1	0.1	308.8	0.0	-3.0
4.5	2		-61110.4	1617.7	3202.7	1	0.1	308.8	0.0	-3.0
5.0	2		-60956.0	1617.9	3194.6	1	0.1	308.8	0.0	-3.0

TABLE B4.-Run.track Output File

*ESA
run1
*FLOAT

T0	DISTshad	DISTshad_MIN	DIST	DIST_MIN	CLOSING_RATE
0.5	4531.5	4531.5	4531.5	4531.5	30.2
1.0	4516.5	4516.5	4516.5	4516.5	30.0
1.5	4501.5	4501.5	4501.5	4501.5	29.8
2.0	4486.7	4486.7	4486.7	4486.7	29.6
2.5	4472.0	4472.0	4472.0	4472.0	29.4
3.0	4457.4	4457.4	4457.4	4457.4	29.1
3.5	4442.8	4442.8	4442.8	4442.8	28.9
4.0	4428.4	4428.4	4428.4	4428.4	28.7
4.5	4414.1	4414.1	4414.1	4414.1	28.5
5.0	4400.0	4400.0	4400.0	4400.0	28.3
5.5	4385.9	4385.9	4385.9	4385.9	28.0
6.0	4371.9	4371.9	4371.9	4371.9	27.8
6.5	4358.1	4358.1	4358.1	4358.1	27.6
7.0	4344.3	4344.3	4344.3	4344.3	27.4
7.5	4330.7	4330.7	4330.7	4330.7	27.1
8.0	4317.2	4317.2	4317.2	4317.2	26.9
8.5	4303.8	4303.8	4303.8	4303.8	26.6
9.0	4290.6	4290.6	4290.6	4290.6	26.4
9.5	4277.4	4277.4	4277.4	4277.4	26.2
10.0	4264.4	4264.4	4264.4	4264.4	25.9
10.5	4251.5	4251.5	4251.5	4251.5	25.7
11.0	4238.7	4238.7	4238.7	4238.7	25.4
11.5	4224.5	4224.5	4224.5	4224.5	31.7
12.0	4207.0	4207.0	4207.0	4207.0	38.5
12.5	4186.1	4186.1	4186.1	4186.1	45.2
13.0	4161.8	4161.8	4161.8	4161.8	51.9
13.5	4134.2	4134.2	4134.2	4134.2	58.5
14.0	4103.4	4103.4	4103.4	4103.4	65.0
14.5	4069.3	4069.3	4069.3	4069.3	71.4
15.0	4032.0	4032.0	4032.0	4032.0	77.8
15.5	3991.6	3991.6	3991.6	3991.6	84.0
16.0	3948.0	3948.0	3948.0	3948.0	90.1
16.5	3901.5	3901.5	3901.5	3901.5	96.1
17.0	3851.9	3851.9	3851.9	3851.9	102.0
17.5	3799.5	3799.5	3799.5	3799.5	107.7
18.0	3744.3	3744.3	3744.3	3744.3	113.2
18.5	3686.3	3686.3	3686.3	3686.3	118.5
19.0	3625.8	3625.8	3625.8	3625.8	123.7
19.5	3562.7	3562.7	3562.7	3562.7	128.5
20.0	3497.3	3497.3	3497.3	3497.3	133.1
20.5	3429.7	3429.7	3429.7	3429.7	137.4
21.0	3360.0	3360.0	3360.0	3360.0	141.0
21.5	3289.6	3289.6	3289.6	3289.6	140.5
22.0	3219.5	3219.5	3219.5	3219.5	139.9
22.5	3149.7	3149.7	3149.7	3149.7	139.3
23.0	3080.3	3080.3	3080.3	3080.3	138.6
23.5	3011.1	3011.1	3011.1	3011.1	137.9
24.0	2942.4	2942.4	2942.4	2942.4	137.1
24.5	2874.0	2874.0	2874.0	2874.0	136.3
25.0	2806.1	2806.1	2806.1	2806.1	135.5
25.5	2738.5	2738.5	2738.5	2738.5	134.5
26.0	2671.5	2671.5	2671.5	2671.5	133.5
26.5	2605.0	2605.0	2605.0	2605.0	132.4
27.0	2539.1	2539.1	2540.4	2540.4	131.3
27.5	2473.8	2473.8	2478.9	2478.9	130.0
28.0	2409.1	2409.1	2420.5	2420.5	128.6
28.5	2345.2	2345.2	2365.0	2365.0	127.2
29.0	2282.0	2282.0	2312.4	2312.4	125.5
29.5	2219.6	2219.6	2262.4	2262.4	123.8
30.0	2158.2	2158.2	2215.1	2215.1	121.9
30.5	2097.8	2097.8	2170.1	2170.1	119.8
31.0	2038.4	2038.4	2127.5	2127.5	117.6
31.5	1980.2	1980.2	2087.0	2087.0	115.1
32.0	1923.3	1923.3	2048.5	2048.5	112.4
32.5	1867.8	1867.8	2011.9	2011.9	109.5
33.0	1813.8	1813.8	1977.1	1977.1	106.3
33.5	1761.5	1761.5	1943.8	1943.8	102.8
34.0	1711.1	1711.1	1911.9	1911.9	99.0

34.5	1662.6	1662.6	1881.5	1881.5	94.9
35.0	1616.2	1616.2	1852.2	1852.2	90.4
35.5	1572.3	1572.3	1824.1	1824.1	85.4
36.0	1530.9	1530.9	1797.0	1797.0	80.1
36.5	1492.2	1492.2	1770.9	1770.9	74.3
37.0	1456.6	1456.6	1745.6	1745.6	68.1
37.5	1424.2	1424.2	1721.3	1721.3	61.4
38.0	1395.2	1395.2	1697.8	1697.8	54.3
38.5	1369.9	1369.9	1675.1	1675.1	46.8
39.0	1348.5	1348.5	1653.3	1653.3	38.9
39.5	1331.1	1331.1	1632.3	1632.3	30.6
40.0	1318.0	1318.0	1612.4	1612.4	22.0
40.5	1309.2	1309.2	1593.6	1593.6	13.2
41.0	1304.8	1304.8	1576.0	1576.0	4.3
41.5	1304.9	1304.8	1559.7	1559.7	-4.7
42.0	1309.5	1304.8	1545.0	1545.0	-13.6
42.5	1318.5	1304.8	1532.0	1532.0	-22.4
43.0	1331.9	1304.8	1521.0	1521.0	-31.0
43.5	1349.4	1304.8	1512.3	1512.3	-39.2
44.0	1371.0	1304.8	1506.1	1506.1	-47.2
44.5	1396.5	1304.8	1502.7	1502.7	-54.7
45.0	1425.7	1304.8	1502.5	1502.5	-61.8
45.5	1458.2	1304.8	1505.5	1502.5	-68.4
46.0	1494.0	1304.8	1511.7	1502.5	-74.6
46.5	1532.8	1304.8	1520.9	1502.5	-80.4
47.0	1574.3	1304.8	1533.1	1502.5	-85.7
47.5	1618.4	1304.8	1548.2	1502.5	-90.6
48.0	1664.8	1304.8	1566.2	1502.5	-95.1
48.5	1713.4	1304.8	1586.9	1502.5	-99.2
49.0	1764.0	1304.8	1610.3	1502.5	-103.0
49.5	1816.3	1304.8	1636.3	1502.5	-106.5
50.0	1870.4	1304.8	1664.6	1502.5	-109.7
50.5	1926.0	1304.8	1695.2	1502.5	-112.6
51.0	1982.9	1304.8	1728.0	1502.5	-115.2
51.5	2041.2	1304.8	1762.9	1502.5	-117.7
52.0	2100.6	1304.8	1799.7	1502.5	-119.9
52.5	2161.1	1304.8	1838.3	1502.5	-122.0
53.0	2222.6	1304.8	1878.6	1502.5	-123.9
53.5	2284.9	1304.8	1920.5	1502.5	-125.6
54.0	2348.2	1304.8	1963.9	1502.5	-127.2
54.5	2412.1	1304.8	2008.7	1502.5	-128.7
55.0	2476.8	1304.8	2054.8	1502.5	-130.1
55.5	2542.2	1304.8	2102.1	1502.5	-131.3
56.0	2608.2	1304.8	2150.5	1502.5	-132.5
56.5	2674.7	1304.8	2200.1	1502.5	-133.6
57.0	2741.7	1304.8	2250.6	1502.5	-134.6
57.5	2809.3	1304.8	2302.0	1502.5	-135.5
58.0	2877.2	1304.8	2354.3	1502.5	-136.4
58.5	2945.6	1304.8	2407.5	1502.5	-137.2
59.0	3014.4	1304.8	2461.3	1502.5	-137.9
59.5	3083.5	1304.8	2515.9	1502.5	-138.6
60.0	3153.0	1304.8	2571.2	1502.5	-139.3
60.5	3222.8	1304.8	2627.1	1502.5	-139.9
61.0	3292.9	1304.8	2683.5	1502.5	-140.5
61.5	3363.3	1304.8	2740.5	1502.5	-141.0
62.0	3434.0	1304.8	2798.0	1502.5	-141.5
62.5	3504.9	1304.8	2856.1	1502.5	-142.0
63.0	3576.0	1304.8	2914.5	1502.5	-142.5
63.5	3647.3	1304.8	2973.4	1502.5	-142.9
64.0	3718.9	1304.8	3032.7	1502.5	-143.3
64.5	3790.6	1304.8	3092.4	1502.5	-143.7
65.0	3862.5	1304.8	3152.4	1502.5	-144.0
65.5	3934.6	1304.8	3212.7	1502.5	-144.4
66.0	4006.9	1304.8	3273.4	1502.5	-144.7
66.5	4079.3	1304.8	3334.4	1502.5	-145.0
67.0	4151.8	1304.8	3395.7	1502.5	-145.3
67.5	4224.5	1304.8	3457.2	1502.5	-145.5
68.0	4297.4	1304.8	3519.0	1502.5	-145.8
68.5	4370.3	1304.8	3581.1	1502.5	-146.0
69.0	4443.4	1304.8	3643.3	1502.5	-146.3
69.5	4516.6	1304.8	3705.8	1502.5	-146.5
70.0	4589.9	1304.8	3768.5	1502.5	-146.7

70.5	4663.3	1304.8	3831.4	1502.5	-146.9
71.0	4736.8	1304.8	3894.5	1502.5	-147.1
71.5	4810.3	1304.8	3957.8	1502.5	-147.3
72.0	4884.0	1304.8	4021.2	1502.5	-147.4
72.5	4957.8	1304.8	4084.8	1502.5	-147.6
73.0	5031.6	1304.8	4148.5	1502.5	-147.8
73.5	5105.6	1304.8	4212.4	1502.5	-147.9
74.0	5179.6	1304.8	4276.5	1502.5	-148.1
74.5	5253.6	1304.8	4340.7	1502.5	-148.2
75.0	5327.8	1304.8	4405.0	1502.5	-148.3
75.5	5402.0	1304.8	4469.4	1502.5	-148.5
76.0	5476.3	1304.8	4533.9	1502.5	-148.6
76.5	5550.6	1304.8	4598.6	1502.5	-148.7

*ESA

run1

*FLOAT

TO	DISTshad	DISTshad_MIN	DIST	DIST_MIN	CLOSING_RATE
0.5	4342.7	4342.7	4342.7	4342.7	-4.6
1.0	4345.0	4342.7	4345.0	4342.7	-4.6
1.5	4347.3	4342.7	4347.3	4342.7	-4.6
2.0	4349.6	4342.7	4349.6	4342.7	-4.7
2.5	4352.0	4342.7	4352.0	4342.7	-4.7
3.0	4354.3	4342.7	4354.3	4342.7	-4.7
3.5	4356.6	4342.7	4356.6	4342.7	-4.7
4.0	4359.0	4342.7	4359.0	4342.7	-4.7
4.5	4361.3	4342.7	4361.3	4342.7	-4.7
5.0	4363.7	4342.7	4363.7	4342.7	-4.7

BIBLIOGRAPHY

1. Boeing Commercial Airplane Group, Development and Exercise of an Analytical Model of the Air Traffic System, D6-60132, January 1971.
2. Federal Aviation Administration, *Precision Runway Monitor Demonstration Report*, Department of Transportation Report, DOT/FAA/RD-91/5, February 1991.
3. A.L. Hainers and W.J. Swedish, *Requirements for Independent and Dependent Parallel Instrument Approaches at Reduced Runway Spacing*, MITRE Corporation, FAA EM-81-8, May 1981.
4. *Precision Runway Monitor Quarterly Technical Letter*, MIT Lincoln Laboratory, 42QTL-PRM-90-02, 29 May 1990.
5. K. Hollister, *Blunder Risk Model, Version 1.0*, MIT Lincoln Laboratory, 42PM-PRM-001, 23 January 1992.
6. S.V. Massimini, *The Blunder Resolutions Performance Model*, MITRE Corporation, 91W00147, 1991.

REPORT DOCUMENTATION PAGE			Form Approved OMB No. 0704-0188	
Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.				
1. AGENCY USE ONLY (Leave blank)		2. REPORT DATE December 1993		3. REPORT TYPE AND DATES COVERED Contractor Report
4. TITLE AND SUBTITLE Parallel Runway Requirement Analysis Study Volume 2 - Simulation Model			5. FUNDING NUMBERS CNAS1-18027 WU505-66-41-04	
6. AUTHOR(S) Yaghoob S. Ebrahimi and Ken S. Chun				
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) Boeing Commercial Airplane Group P.O. Box 3707 M/S 7X-MR Seattle, WA 98124-2207			8. PERFORMING ORGANIZATION REPORT NUMBER NASA CR191549 Volume 2 - Volume 2	
9. SPONSORING / MONITORING AGENCY NAME(S) AND ADDRESS(ES) National Aeronautics and Space Administration Langley Research Center Hampton, VA 23665-5225			10. SPONSORING / MONITORING AGENCY REPORT NUMBER	
11. SUPPLEMENTARY NOTES Langley Technical Monitor: Leonard Credeur Langley Contracting Officer's Technical Representative: Cary P. Spitzer Final Report - Task 25				
12a. DISTRIBUTION / AVAILABILITY STATEMENT Unclassified - Unlimited Subject Category 04			12b. DISTRIBUTION CODE	
13. ABSTRACT (Maximum 200 words) This document is a user manual for operating the PLAND_BLUNDER (PLB) simulation program. This simulation is based on two aircraft approaching parallel runways independently and using parallel Instrument Landing System (ILS) equipment during Instrument Meteorological Conditions (IMC). If an aircraft should deviate from its assigned localizer course toward the opposite runway, this constitutes a <i>blunder</i> which could endanger the aircraft on the adjacent path. The worst case scenario would be if the blundering aircraft were unable to recover and continue toward the adjacent runway. PLAND_BLUNDER is a Monte Carlo-type simulation which employs the events and aircraft positioning during such a <i>blunder situation</i> . The model simulates two aircraft performing parallel ILS approaches using IMC or visual procedures. PLB uses a simple movement model and control law in three dimensions (X, Y, Z). The parameters of the simulation inputs and outputs are defined in this document along with a sample of the statistical analysis. This document is the second volume of a two volume set. Volume 1 is a description of the application of the PLB to the analysis of close parallel runway operations.				
14. SUBJECT TERMS Parallel Runway Approaches, Parallel Runway ILS Approaches, Parametric Simulation Model for Parallel Runways			15. NUMBER OF PAGES 47	
			16. PRICE CODE A04	
17. SECURITY CLASSIFICATION OF REPORT Unclassified	18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified	19. SECURITY CLASSIFICATION OF ABSTRACT	20. LIMITATION OF ABSTRACT	

